

Project Specific Hydrology / Hydraulics Report

FOR:

***PRELIMINARY GRADING FOR
CENTERPOINTE 78
990 North Broadway
Escondido, CA 92026***

PREPARED FOR:

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501 Santa Monica Blvd, Suite 312
Santa Monica, CA 90401***

PREPARED BY:

***EXCEL ENGINEERING
440 State Place
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Engineer of Work
Project No: 12-005***

DATE PREPARED:

April 3, 2013

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1.0 PROJECT DESCRIPTION AND PURPOSE

The purposes of this project are to develop a multi retail center improve the water quality and on-site drainage system, and to analyze the proposed facilities associated with this project to ensure that downstream or offsite properties will not be adversely affected by our project's proposed development. The improvements are: parking lots, buildings, and drainage facilities. Drainage facilities, such as the bio-retention basins, are utilized for water quality purposes. Please see Water Quality Report prepared by Excel Engineering, dated ____.

2.0 VICINITY MAP

The project site is located on North Broadway, in between Lincoln Avenue and Highway 78 in Escondido, San Diego County, CA. Please see Attachment A- Vicinity map.

3.0 SITE MAP

Please see Attachment B – Site map

4.0 DESCRIPTION OF WATERSHED

4.1 Existing Conditions Topography

The project site is an existing car lot, which consists of office buildings, car garages, retaining walls, asphalt parking lots, concrete gutters, and minimal vegetation. It's approximately 3.69 acres, bounded on the west by residential housing, north by Lincoln Avenue, North Broadway on the east, and an earthen swale and Highway 78 to the south. The site consists of parcels in a rectangular shape, located north of Highway 78, in the City of Escondido.

The existing conditions are divided into 6 separate tributary basins, which are labeled as Basin A, B, C, D, E, and F. Much of the storm water flows over the asphalt parking lots, collected in concrete gutters, and then routed to Lincoln Avenue. The southeast area of the existing site flows over land and into an existing curb inlet at the corner of North Broadway and Highway 78. The southwest and southern portions flow over land and into an existing brow ditch, located in between Highway 78 and the project site.

Land use in the surrounding areas is predominantly zoned for commercial development. The soil type in this area is predominantly type "D."
For more features of the site, please see Attachment D – Watershed Information Topographic Maps: Pre-Development Map.

4.2 Existing Conditions + Project Conditions Topography

For the purpose of hydrologic analysis, the project is divided into five large tributary basins designated as Basin A, B, C, D, and E. And 3 smaller tributary

basins designated as Basin B1, C1, and E1. The flow generated on basins A, B, and C will be directed to bio-retention facilities parallel to Lincoln Avenue. Flow from Basin D enters a bio-retention facility on the southern side of the project site. The discharge from these bio-retention facilities are routed to the northeast corner of the site, where it will connect to a proposed storm drain cleanout structure, which eventually ties into the existing storm drain system at the northwest corner of North Broadway and Lincoln Ave. The storm water from the loading dock and receiving area on the southwest corner of the project is Basin E and is directed to a flume shaped structure. Two, 60-inch Bio Clean Flume Filters will be installed within the flume shaped structure. Please see Attachment F for the Bio Clean Flume Filter details. Basin C1 storm water is routed to a bio-retention facility on the southeast corner of the site, where it eventually discharges onto North Broadway and to an existing catch basin on the corner of North Broadway and Highway 78. Both Basins B1 and E1 storm water flows overland and onto Lincoln Ave. Please see Attachment D – Watershed Information Topographic Maps: Post-Development Map.

4.3 Hydrologic Unit Contribution

The project is within the Carlsbad Hydrologic Unit (904), Escondido Creek HA (904.6), and Escondido HSA (904.62)
Impaired Receiving Water Bodies – Escondido Creek
303(d) Listed Pollutant / Stressor – DDT, Manganese, Phosphate, Selenium, Sulfates, and Total Dissolved Solid.

5.0 METHODOLOGY

This study complies with the 2003 San Diego Hydrology Manual and City of Escondido Design and Standard Drawing. The Rational Method, as presented in section 3, workbook examples, and Escondido C factor and T_C were utilized.

5.1 Hydrology Software

The “Rational Hydrology Method, San Diego County (2003 Manual)” module of the *CIVILCADD/CIVIL DESIGN* Engineering software version 7.4 is used in this study. This software was also used to develop hydrographs from the Rational Method results. This procedure also complies with the 2003 San Diego Hydrology Manual as presented in Section 6.

6.0 CALCULATIONS

6.1 Determine the Watersheds that affect the project

Please see the “Watershed Topographic Maps” for both the “Pre & Post Development” conditions in Attachment D.

6.2 Analyze 2 Year & 50 Year - 6 Hour Storm using Rational Method

Please see “Pre & Post Development Hydrologic 2 Year & 50 Year 6 Hour Storm Analysis” in Attachment E for the details & printouts of the calculation involved in determining the runoffs for both the 2 year & 50 year, 6 hour storm.

6.3 Analyze Q₂ and Q₅₀ Year Storm using Hydrograph

In order for this project to comply with the City of Escondido Water Quality requirements as outlined in Drainage Design Standard, Section 1 through 5, the 2 & 50 years 6 hour storm is analyzed.

6.4 Analyses and Recapitulation

For the existing condition, much of the storm water flows north towards Lincoln Avenue. The remaining storm water flows south towards Highway 78 and the landscaping in between the project site and Highway 78. This assumption is considered per existing gutters, buildings, and topography. In the post development, there will be similar outfalls.

In the Post development condition mentioned above, there are five, large tributary areas labeled as Basin A, B, C, D and E. And three smaller tributary areas labeled as Basin B1, C1, and E1. Basin A (1.091 Acres) and Basin B (0.727 Acres) are directed to bio-retention facilities. Basin C (0.486 Acres) flows to a bio-retention facility on the southeast corner of the project site. Basin D (0.735 Acres) enters a bio-retention facility on the southern side of the project site and is routed north, where it connects with the drainage system that collects the discharge from the bio-retention facilities serving Basins A, B, and C. Eventually, the discharge from Basins A, B, C, and D enter the existing storm drain system on the northwest corner of North Broadway and Lincoln Ave. Basin E (0.36 Acres) flows to a concrete flume structure on the southwest corner of the project and discharges to an existing gutter, which is located in the landscaping between the project site and Highway 78. (Please see attachment E for Hydrology calculation using CivilD program.)

Existing Condition

As we can see from Table 1, the ultimate Q₂ and Q₅₀ peak flows are 11.87cfs and 21.83 cfs, respectively. Existing condition is calculated as a whole area with 3.69 Acres in size.

Table 1. 2 Year and 50 Year Storm Event Peak flows

| | Q (cfs) | | Area (Acres) |
|--------------|--------------|--------------|--------------|
| | 2 Year | 50 Year | |
| | Outfall A | 2.07 | 3.82 |
| Outfall B | 2.08 | 3.83 | 0.634 |
| Outfall C | 4.56 | 8.52 | 0.656 |
| Outfall D | 1.49 | 2.69 | 0.319 |
| Outfall E | 1.62 | 2.88 | 0.342 |
| Outfall F | 0.05 | 0.09 | 0.05 |
| Total | 11.87 | 21.83 | 3.69 |

Post Development Condition

See Table 2 and 3 below for more detail calculations:

Table 2. 2 Year Storm and 50 Year Event Peak flows

| | Q (cfs) | | Area (Acres) |
|--------------|--------------|--------------|--------------|
| | 2 Year | 50 Year | |
| | Outfall A | 8.08 | 14.764 |
| Outfall B | 0.39 | 0.752 | 0.165 |
| Outfall C | 1.06 | 1.966 | 0.36 |
| Outfall D | 0.36 | 0.639 | 0.079 |
| Outfall E | 0.20 | 0.36 | 0.047 |
| Total | 10.09 | 18.48 | 3.69 |

Table 3. Runoff Recapitulation

| | 2 Year Storm | | 50 Year Storm | |
|---------------------|--------------|-------|---------------|-------|
| | Pre | Post | Pre | Post |
| Q Peak runoff (cfs) | 11.87 | 10.09 | 21.83 | 18.48 |
| | | | | |

Table 3 shows that the peak flows of the 2 and 50 year storm of the Post-development are less than that of the Pre-Development.

7.0 SUMMARY

This Hydrology/Hydraulic report is prepared to evaluate the conditions of concern for the Centerpointe 78 Project. The site area is approximately 3.69 acres with the majority of the storm water flow going to Lincoln Avenue. On the south of the site there is an existing gutter surrounded by vegetation, which is where the remaining storm water flows to.

From the calculation, the peak flows of the 2 and 50 year storm of the Post-development are less than the Pre-Development peak flows.

As presented in this study, we have shown that this project will not increase storm runoff and thus not adversely affect the existing downstream storm drain facilities.

8.0 REFERENCES

Domingue Edward N., Design Standards and Standard Drawings; City of Escondido
May 6, 2009

City of Escondido; Storm Water Management Requirements and Local Standard Urban
Storm Water Mitigation Plan, November 13, 2002.

California Stormwater Quality Association; Stormwater Best Management Practice
Handbook- New Development and Redevelopment, January 2003.

County of San Diego Department of Public Works; Flood Control Section, Hydrology
Manual; June 2003.

9.0 DECLARATION OF RESPONSIBLE CHARGE

I hereby declare that I am the engineer of work for this project. That I have exercised responsible charge over the design of the project as defined in section 6703 of the business and professions codes, and that the design is consistent with current design.

I understand that the check of the project drawings and specifications by the City of Murrieta is confined to a review only and does not relieve me, as engineer of work, of my responsibilities for project design.

ENGINEER OF WORK

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Tel – (760)745-8118
Fax – (760)745-1890

Project Number: 12-005

Robert D. Dentino, RCE 45629
Registration Expire: December 31, 2014

Date

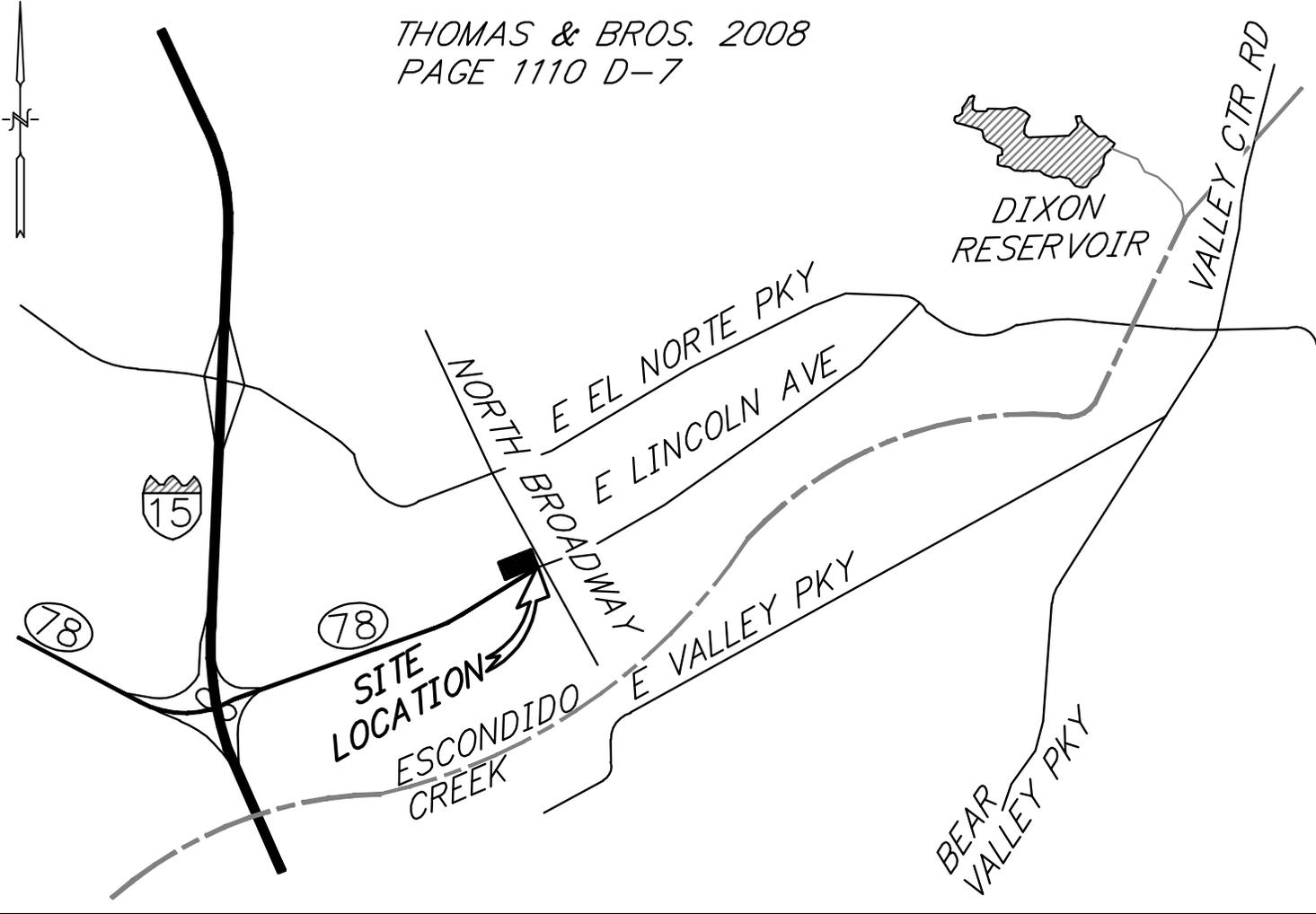
ATTACHMENTS

VICINITY MAP

ATTACHMENT A

VICINITY MAP

THOMAS & BROS. 2008
PAGE 1110 D-7



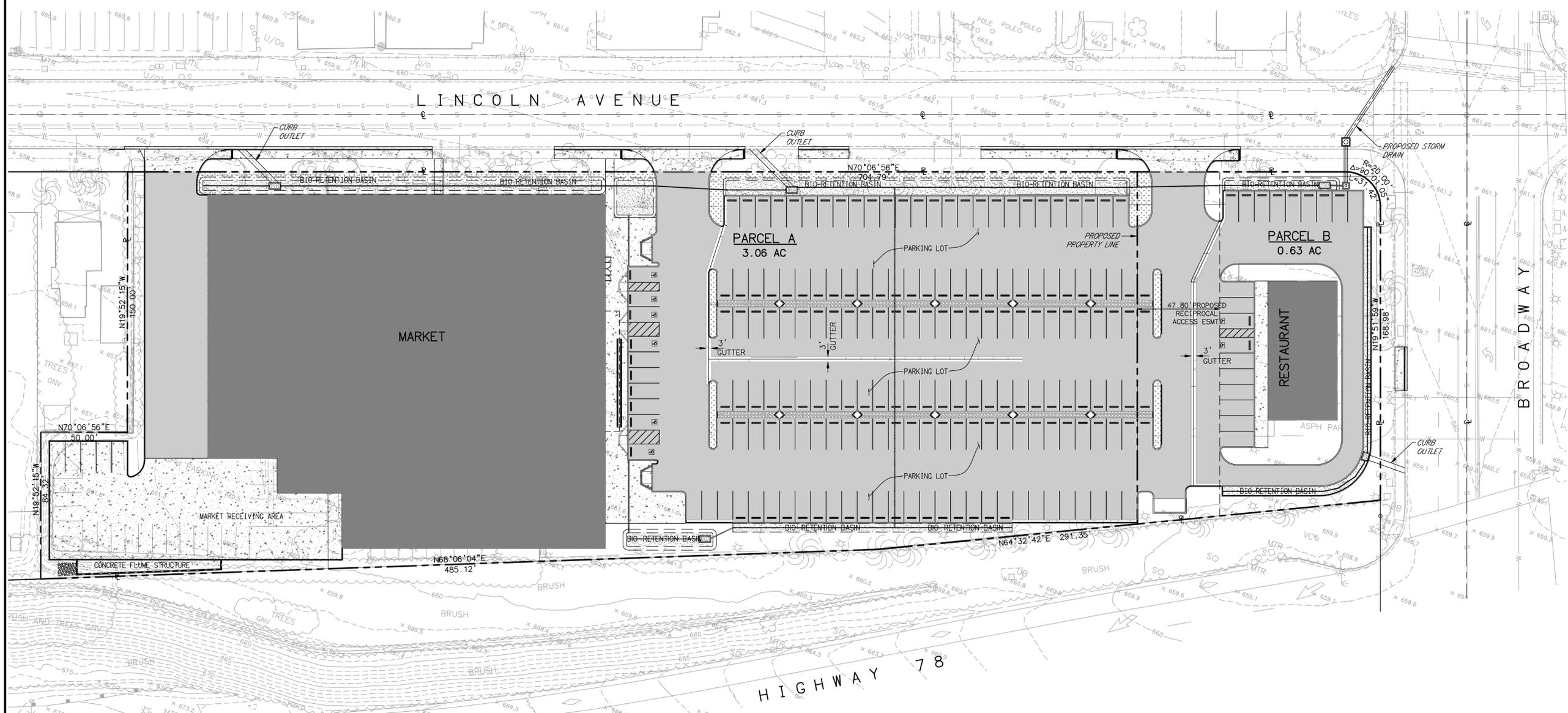
ATTACHMENT B

SITE MAP

See 36"x24" map at the attached pocket

SITE MAP

990 NORTH BROADWAY ESCONDIDO, CA



ABBREVIATIONS

| | |
|-----|-----------------------|
| P/L | PROPERTY LINE |
| R/W | RIGHT OF WAY |
| C/L | CENTERLINE |
| TC | TOP OF CURB |
| FL | FLOWLINE |
| TG | TOP OF GRATE |
| GB | GRADE BREAK |
| FG | FINISH GRADE |
| FS | FINISH SURFACE |
| HP | HIGH POINT |
| IE | INVERT OF DRAIN |
| PAD | PAD ELEVATION |
| FF | FINISH FLOOR |
| BVC | BEGIN VERTICLE CURVE |
| EVC | END VERTICLE CURVE |
| PI | POINT OF INTERSECTION |
| EP | EDGE OF PAVEMENT |
| TW | TOP OF WALL |
| TF | TOP OF FOOTING |

LEGENDS & SYMBOLS

| | |
|--|----------------------|
| | PROPERTY LINE |
| | RIGHT OF WAY |
| | CURB LINE |
| | CURB & GUTTER |
| | EXIST. CONTOUR |
| | PROP. CONTOUR |
| | TOP & TOE OF SLOPE |
| | DAYLIGHT LINE |
| | DIRECTION OF FLOW |
| | GRADE |
| | VEHICLE WHEEL STOP |
| | PARKING SPACE NUMBER |
| | STORM DRAIN PIPE |

LEGENDS & SYMBOLS

| | |
|--|-------------------------|
| | EXIST. WATERLINE |
| | EXIST. GAS LINE |
| | EXIST. SEWER LINE |
| | EXIST. TELEPHONE LINE |
| | EXIST. ELECTRICITY LINE |
| | EXIST. STREET LIGHT |
| | EXIST. FIRE HYDRANT |
| | WATER LINE |
| | GAS LINE |
| | SEWER LINE |
| | TELEPHONE LINE |
| | ELECTRICITY LINE |
| | PROP. FIRE HYDRANT |
| | WATER SERVICE |
| | SEWER SERVICE |
| | PROP. STREET LIGHT |

| | |
|--|---------------------|
| | BIO-RETENTION BASIN |
| | LANDSCAPE AREA |
| | ASPHALT PAVEMENT |



SCALE: 1"=30'

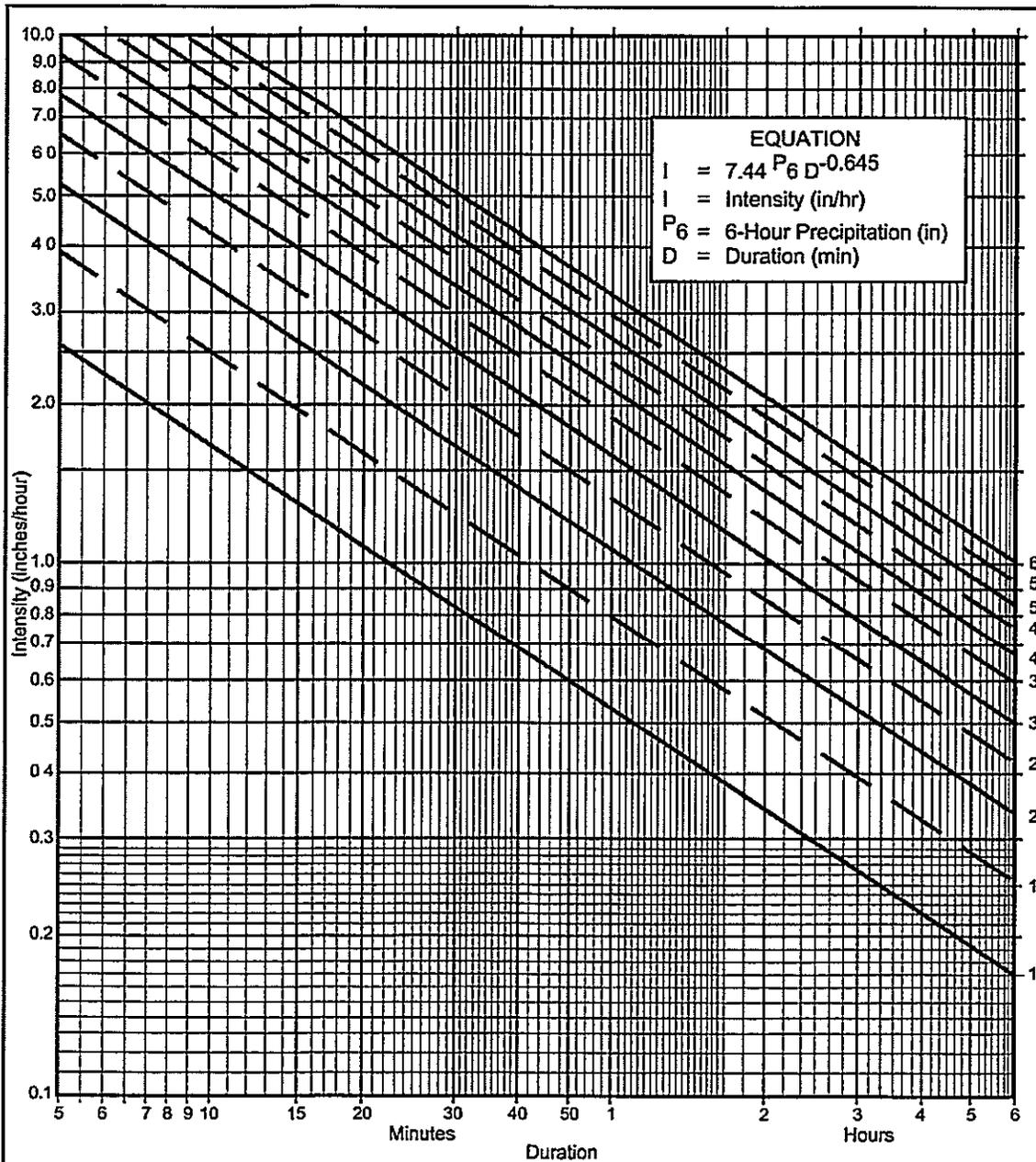


**CENTERPOINTE 78
SITE MAP**
 APN 229-121-08, 09, 10, 11,
 12, 13, 14, 15
 SITE ADDRESS: 990 NORTH BROADWAY
 ESCONDIDO, CA 92026



ATTACHMENT C

FIGURES & TABLES FROM SAN DIEGO COUNTY HYDROLOGY MANUAL



Directions for Application:

- (1) From precipitation maps determine 6 hr and 24 hr amounts for the selected frequency. These maps are included in the County Hydrology Manual (10, 50, and 100 yr maps included in the Design and Procedure Manual).
- (2) Adjust 6 hr precipitation (if necessary) so that it is within the range of 45% to 65% of the 24 hr precipitation (not applicable to Desert).
- (3) Plot 6 hr precipitation on the right side of the chart.
- (4) Draw a line through the point parallel to the plotted lines.
- (5) This line is the intensity-duration curve for the location being analyzed.

Application Form:

- (a) Selected frequency _____ year
- (b) $P_6 =$ _____ in., $P_{24} =$ _____, $\frac{P_6}{P_{24}} =$ _____ %⁽²⁾
- (c) Adjusted $P_6^{(2)} =$ _____ in.
- (d) $t_x =$ _____ min.
- (e) $i =$ _____ in./hr.

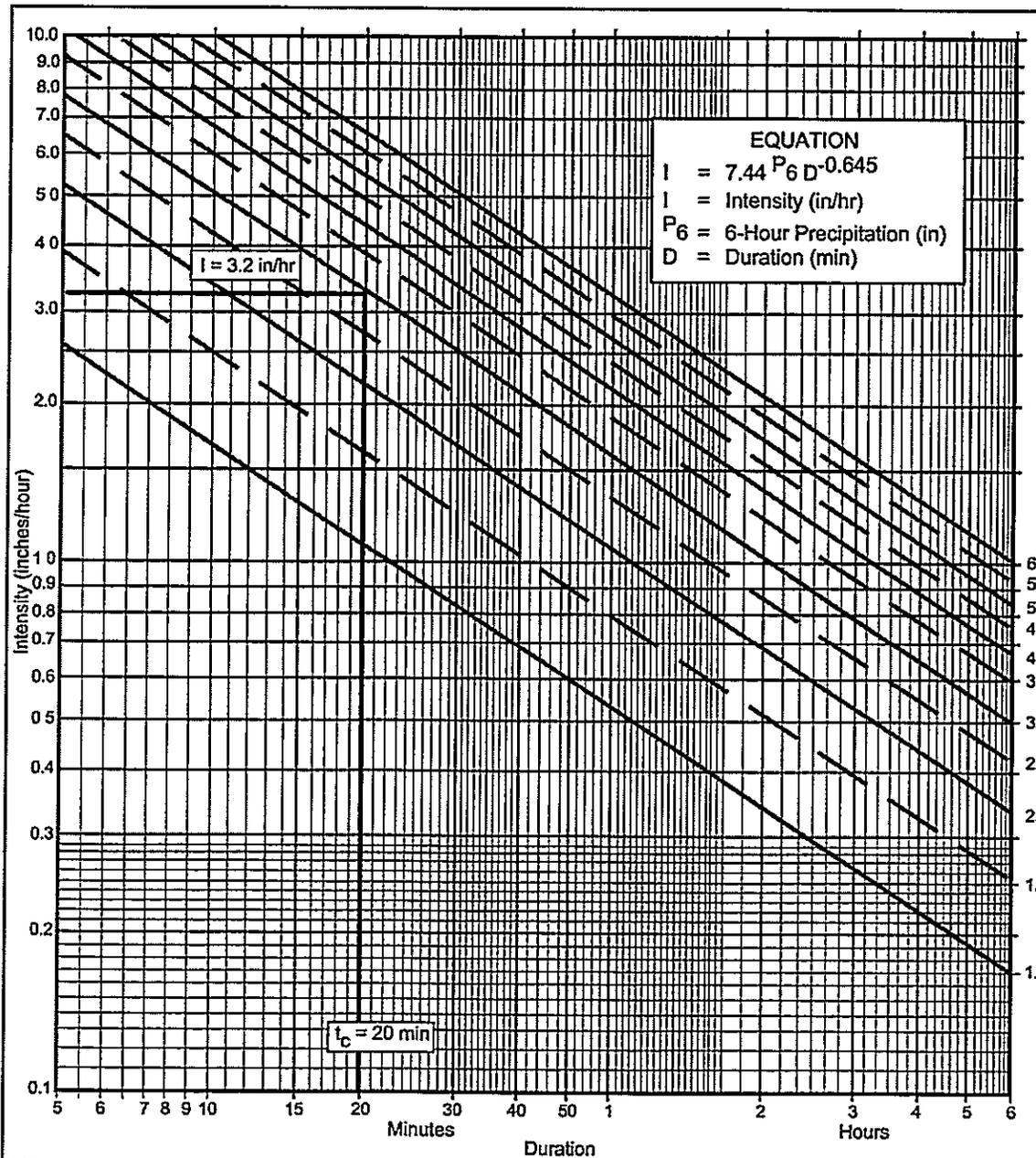
Note: This chart replaces the Intensity-Duration-Frequency curves used since 1965.

| P6 | 1 | 1.5 | 2 | 2.5 | 3 | 3.5 | 4 | 4.5 | 5 | 5.5 | 6 |
|----------|------|------|------|------|------|------|-------|-------|-------|-------|-------|
| Duration | i | i | i | i | i | i | i | i | i | i | i |
| 5 | 2.63 | 3.95 | 5.27 | 6.59 | 7.90 | 9.22 | 10.54 | 11.86 | 13.17 | 14.49 | 15.81 |
| 7 | 2.12 | 3.18 | 4.24 | 5.30 | 6.36 | 7.42 | 8.48 | 9.54 | 10.60 | 11.66 | 12.72 |
| 10 | 1.68 | 2.53 | 3.37 | 4.21 | 5.05 | 5.90 | 6.74 | 7.58 | 8.42 | 9.27 | 10.11 |
| 15 | 1.30 | 1.95 | 2.59 | 3.24 | 3.89 | 4.54 | 5.19 | 5.84 | 6.49 | 7.13 | 7.78 |
| 20 | 1.08 | 1.62 | 2.15 | 2.69 | 3.23 | 3.77 | 4.31 | 4.85 | 5.39 | 5.93 | 6.46 |
| 25 | 0.93 | 1.40 | 1.87 | 2.33 | 2.80 | 3.27 | 3.73 | 4.20 | 4.67 | 5.13 | 5.60 |
| 30 | 0.83 | 1.24 | 1.66 | 2.07 | 2.49 | 2.90 | 3.32 | 3.73 | 4.15 | 4.56 | 4.98 |
| 40 | 0.69 | 1.03 | 1.38 | 1.72 | 2.07 | 2.41 | 2.76 | 3.10 | 3.45 | 3.79 | 4.13 |
| 50 | 0.60 | 0.90 | 1.19 | 1.49 | 1.79 | 2.09 | 2.39 | 2.69 | 2.98 | 3.28 | 3.58 |
| 60 | 0.53 | 0.80 | 1.06 | 1.33 | 1.59 | 1.86 | 2.12 | 2.39 | 2.65 | 2.92 | 3.18 |
| 90 | 0.41 | 0.61 | 0.82 | 1.02 | 1.23 | 1.43 | 1.63 | 1.84 | 2.04 | 2.25 | 2.45 |
| 120 | 0.34 | 0.51 | 0.68 | 0.85 | 1.02 | 1.19 | 1.36 | 1.53 | 1.70 | 1.87 | 2.04 |
| 150 | 0.29 | 0.44 | 0.59 | 0.73 | 0.88 | 1.03 | 1.18 | 1.32 | 1.47 | 1.62 | 1.76 |
| 180 | 0.26 | 0.39 | 0.52 | 0.65 | 0.78 | 0.91 | 1.04 | 1.18 | 1.31 | 1.44 | 1.57 |
| 240 | 0.22 | 0.33 | 0.43 | 0.54 | 0.65 | 0.76 | 0.87 | 0.98 | 1.08 | 1.19 | 1.30 |
| 300 | 0.19 | 0.28 | 0.38 | 0.47 | 0.56 | 0.66 | 0.75 | 0.85 | 0.94 | 1.03 | 1.13 |
| 360 | 0.17 | 0.25 | 0.33 | 0.42 | 0.50 | 0.58 | 0.67 | 0.75 | 0.84 | 0.92 | 1.00 |

Intensity-Duration Design Chart - Template

FIGURE

3-1



Directions for Application:

- (1) From precipitation maps determine 6 hr and 24 hr amounts for the selected frequency. These maps are included in the County Hydrology Manual (10, 50, and 100 yr maps included in the Design and Procedure Manual).
- (2) Adjust 6 hr precipitation (if necessary) so that it is within the range of 45% to 65% of the 24 hr precipitation (not applicable to Desert).
- (3) Plot 6 hr precipitation on the right side of the chart.
- (4) Draw a line through the point parallel to the plotted lines.
- (5) This line is the intensity-duration curve for the location being analyzed.

Application Form:

- (a) Selected frequency 50 year
- (b) $P_6 = 3$ in., $P_{24} = 5.5$, $\frac{P_6}{P_{24}} = 54.5$ %⁽²⁾
- (c) Adjusted $P_6^{(2)} = 3$ in.
- (d) $t_x = 20$ min.
- (e) $I = 3.2$ in./hr.

Note: This chart replaces the Intensity-Duration-Frequency curves used since 1965.

| P6 | 1 | 1.5 | 2 | 2.5 | 3 | 3.5 | 4 | 4.5 | 5 | 5.5 | 6 |
|----------|------|------|------|------|------|------|-------|-------|-------|-------|-------|
| Duration | | | | | | | | | | | |
| 5 | 2.63 | 3.95 | 5.27 | 6.59 | 7.90 | 9.22 | 10.54 | 11.86 | 13.17 | 14.49 | 15.81 |
| 7 | 2.12 | 3.18 | 4.24 | 5.30 | 6.36 | 7.42 | 8.48 | 9.54 | 10.60 | 11.66 | 12.72 |
| 10 | 1.68 | 2.53 | 3.37 | 4.21 | 5.05 | 5.90 | 6.74 | 7.58 | 8.42 | 9.27 | 10.11 |
| 15 | 1.30 | 1.95 | 2.59 | 3.24 | 3.89 | 4.54 | 5.19 | 5.84 | 6.49 | 7.13 | 7.78 |
| 20 | 1.08 | 1.62 | 2.15 | 2.69 | 3.23 | 3.77 | 4.31 | 4.85 | 5.39 | 5.93 | 6.46 |
| 25 | 0.93 | 1.40 | 1.87 | 2.33 | 2.80 | 3.27 | 3.73 | 4.20 | 4.67 | 5.13 | 5.60 |
| 30 | 0.83 | 1.24 | 1.66 | 2.07 | 2.49 | 2.90 | 3.32 | 3.73 | 4.15 | 4.56 | 4.98 |
| 40 | 0.69 | 1.03 | 1.38 | 1.72 | 2.07 | 2.41 | 2.76 | 3.10 | 3.45 | 3.79 | 4.13 |
| 50 | 0.60 | 0.90 | 1.19 | 1.49 | 1.79 | 2.09 | 2.39 | 2.69 | 2.98 | 3.28 | 3.58 |
| 60 | 0.53 | 0.80 | 1.06 | 1.33 | 1.59 | 1.86 | 2.12 | 2.39 | 2.65 | 2.92 | 3.18 |
| 90 | 0.41 | 0.61 | 0.82 | 1.02 | 1.23 | 1.43 | 1.63 | 1.84 | 2.04 | 2.25 | 2.45 |
| 120 | 0.34 | 0.51 | 0.68 | 0.85 | 1.02 | 1.19 | 1.36 | 1.53 | 1.70 | 1.87 | 2.04 |
| 150 | 0.29 | 0.44 | 0.59 | 0.73 | 0.88 | 1.03 | 1.18 | 1.32 | 1.47 | 1.62 | 1.76 |
| 180 | 0.26 | 0.39 | 0.52 | 0.65 | 0.78 | 0.91 | 1.04 | 1.18 | 1.31 | 1.44 | 1.57 |
| 240 | 0.22 | 0.33 | 0.43 | 0.54 | 0.65 | 0.76 | 0.87 | 0.98 | 1.08 | 1.19 | 1.30 |
| 300 | 0.19 | 0.28 | 0.38 | 0.47 | 0.56 | 0.66 | 0.75 | 0.85 | 0.94 | 1.03 | 1.13 |
| 360 | 0.17 | 0.25 | 0.33 | 0.42 | 0.50 | 0.58 | 0.67 | 0.75 | 0.84 | 0.92 | 1.00 |

Intensity-Duration Design Chart - Example

FIGURE

3-2

**Table 3-1
RUNOFF COEFFICIENTS FOR URBAN AREAS**

| Land Use | | Runoff Coefficient "C" | | | | |
|---------------------------------------|--------------------------------|------------------------|-----------|------|------|------|
| NRCS Elements | County Elements | % IMPER. | Soil Type | | | |
| | | | A | B | C | D |
| Undisturbed Natural Terrain (Natural) | Permanent Open Space | 0* | 0.20 | 0.25 | 0.30 | 0.35 |
| Low Density Residential (LDR) | Residential, 1.0 DU/A or less | 10 | 0.27 | 0.32 | 0.36 | 0.41 |
| Low Density Residential (LDR) | Residential, 2.0 DU/A or less | 20 | 0.34 | 0.38 | 0.42 | 0.46 |
| Low Density Residential (LDR) | Residential, 2.9 DU/A or less | 25 | 0.38 | 0.41 | 0.45 | 0.49 |
| Medium Density Residential (MDR) | Residential, 4.3 DU/A or less | 30 | 0.41 | 0.45 | 0.48 | 0.52 |
| Medium Density Residential (MDR) | Residential, 7.3 DU/A or less | 40 | 0.48 | 0.51 | 0.54 | 0.57 |
| Medium Density Residential (MDR) | Residential, 10.9 DU/A or less | 45 | 0.52 | 0.54 | 0.57 | 0.60 |
| Medium Density Residential (MDR) | Residential, 14.5 DU/A or less | 50 | 0.55 | 0.58 | 0.60 | 0.63 |
| High Density Residential (HDR) | Residential, 24.0 DU/A or less | 65 | 0.66 | 0.67 | 0.69 | 0.71 |
| High Density Residential (HDR) | Residential, 43.0 DU/A or less | 80 | 0.76 | 0.77 | 0.78 | 0.79 |
| Commercial/Industrial (N. Com) | Neighborhood Commercial | 80 | 0.76 | 0.77 | 0.78 | 0.79 |
| Commercial/Industrial (G. Com) | General Commercial | 85 | 0.80 | 0.80 | 0.81 | 0.82 |
| Commercial/Industrial (O.P. Com) | Office Professional/Commercial | 90 | 0.83 | 0.84 | 0.84 | 0.85 |
| Commercial/Industrial (Limited I.) | Limited Industrial | 90 | 0.83 | 0.84 | 0.84 | 0.85 |
| Commercial/Industrial (General I.) | General Industrial | 95 | 0.87 | 0.87 | 0.87 | 0.87 |

*The values associated with 0% impervious may be used for direct calculation of the runoff coefficient as described in Section 3.1.2 (representing the pervious runoff coefficient, C_p , for the soil type), or for areas that will remain undisturbed in perpetuity. Justification must be given that the area will remain natural forever (e.g., the area is located in Cleveland National Forest).

DU/A = dwelling units per acre

NRCS = National Resources Conservation Service

Note that the Initial Time of Concentration should be reflective of the general land-use at the upstream end of a drainage basin. A single lot with an area of two or less acres does not have a significant effect where the drainage basin area is 20 to 600 acres.

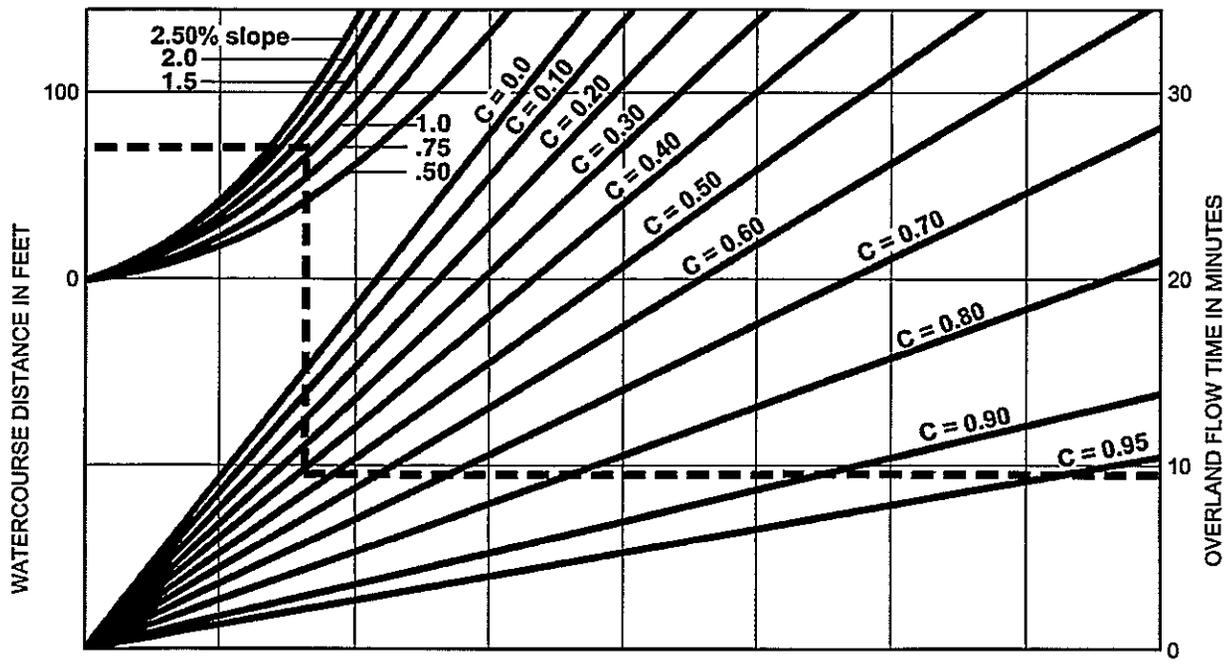
Table 3-2 provides limits of the length (Maximum Length (L_M)) of sheet flow to be used in hydrology studies. Initial T_i values based on average C values for the Land Use Element are also included. These values can be used in planning and design applications as described below. Exceptions may be approved by the "Regulating Agency" when submitted with a detailed study.

Table 3-2

**MAXIMUM OVERLAND FLOW LENGTH (L_M)
& INITIAL TIME OF CONCENTRATION (T_i)**

| Element* | DU/ Acre | .5% | | 1% | | 2% | | 3% | | 5% | | 10% | |
|------------|-------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | | L_M | T_i |
| Natural | | 50 | 13.2 | 70 | 12.5 | 85 | 10.9 | 100 | 10.3 | 100 | 8.7 | 100 | 6.9 |
| LDR | 1 | 50 | 12.2 | 70 | 11.5 | 85 | 10.0 | 100 | 9.5 | 100 | 8.0 | 100 | 6.4 |
| LDR | 2 | 50 | 11.3 | 70 | 10.5 | 85 | 9.2 | 100 | 8.8 | 100 | 7.4 | 100 | 5.8 |
| LDR | 2.9 | 50 | 10.7 | 70 | 10.0 | 85 | 8.8 | 95 | 8.1 | 100 | 7.0 | 100 | 5.6 |
| MDR | 4.3 | 50 | 10.2 | 70 | 9.6 | 80 | 8.1 | 95 | 7.8 | 100 | 6.7 | 100 | 5.3 |
| MDR | 7.3 | 50 | 9.2 | 65 | 8.4 | 80 | 7.4 | 95 | 7.0 | 100 | 6.0 | 100 | 4.8 |
| MDR | 10.9 | 50 | 8.7 | 65 | 7.9 | 80 | 6.9 | 90 | 6.4 | 100 | 5.7 | 100 | 4.5 |
| MDR | 14.5 | 50 | 8.2 | 65 | 7.4 | 80 | 6.5 | 90 | 6.0 | 100 | 5.4 | 100 | 4.3 |
| HDR | 24 | 50 | 6.7 | 65 | 6.1 | 75 | 5.1 | 90 | 4.9 | 95 | 4.3 | 100 | 3.5 |
| HDR | 43 | 50 | 5.3 | 65 | 4.7 | 75 | 4.0 | 85 | 3.8 | 95 | 3.4 | 100 | 2.7 |
| N. Com | | 50 | 5.3 | 60 | 4.5 | 75 | 4.0 | 85 | 3.8 | 95 | 3.4 | 100 | 2.7 |
| G. Com | | 50 | 4.7 | 60 | 4.1 | 75 | 3.6 | 85 | 3.4 | 90 | 2.9 | 100 | 2.4 |
| O.P./Com | | 50 | 4.2 | 60 | 3.7 | 70 | 3.1 | 80 | 2.9 | 90 | 2.6 | 100 | 2.2 |
| Limited I. | | 50 | 4.2 | 60 | 3.7 | 70 | 3.1 | 80 | 2.9 | 90 | 2.6 | 100 | 2.2 |
| General I. | | 50 | 3.7 | 60 | 3.2 | 70 | 2.7 | 80 | 2.6 | 90 | 2.3 | 100 | 1.9 |

*See Table 3-1 for more detailed description



EXAMPLE:
 Given: Watercourse Distance (D) = 70 Feet
 Slope (s) = 1.3%
 Runoff Coefficient (C) = 0.41
 Overland Flow Time (T) = 9.5 Minutes

$$T = \frac{1.8 (1.1-C) \sqrt{D}}{\sqrt[3]{s}}$$

SOURCE: Airport Drainage, Federal Aviation Administration, 1965

Rational Formula - Overland Time of Flow Nomograph

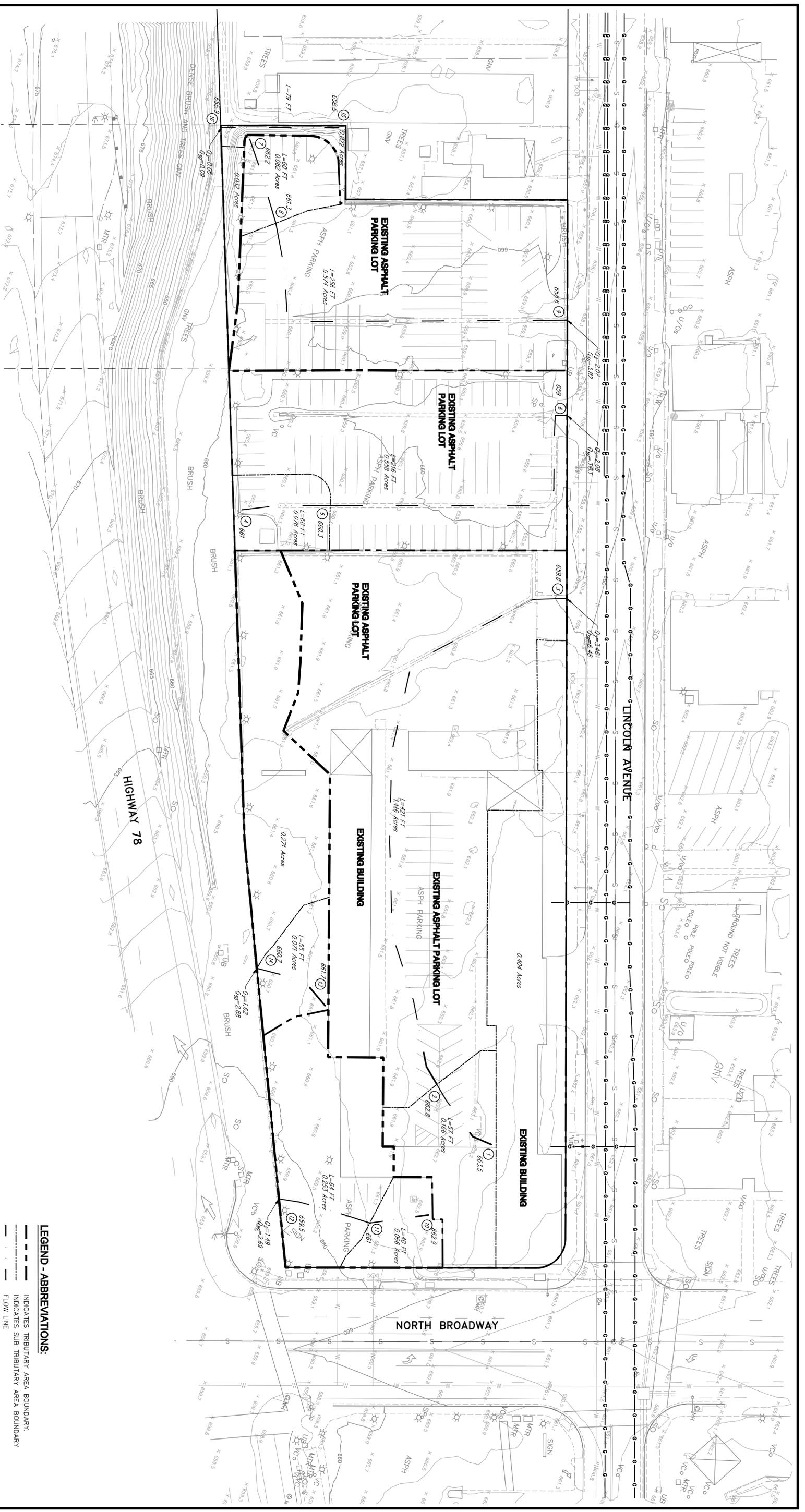
FIGURE

3-3

ATTACHMENT D

WATERSHED INFORMATION

Topographic Maps

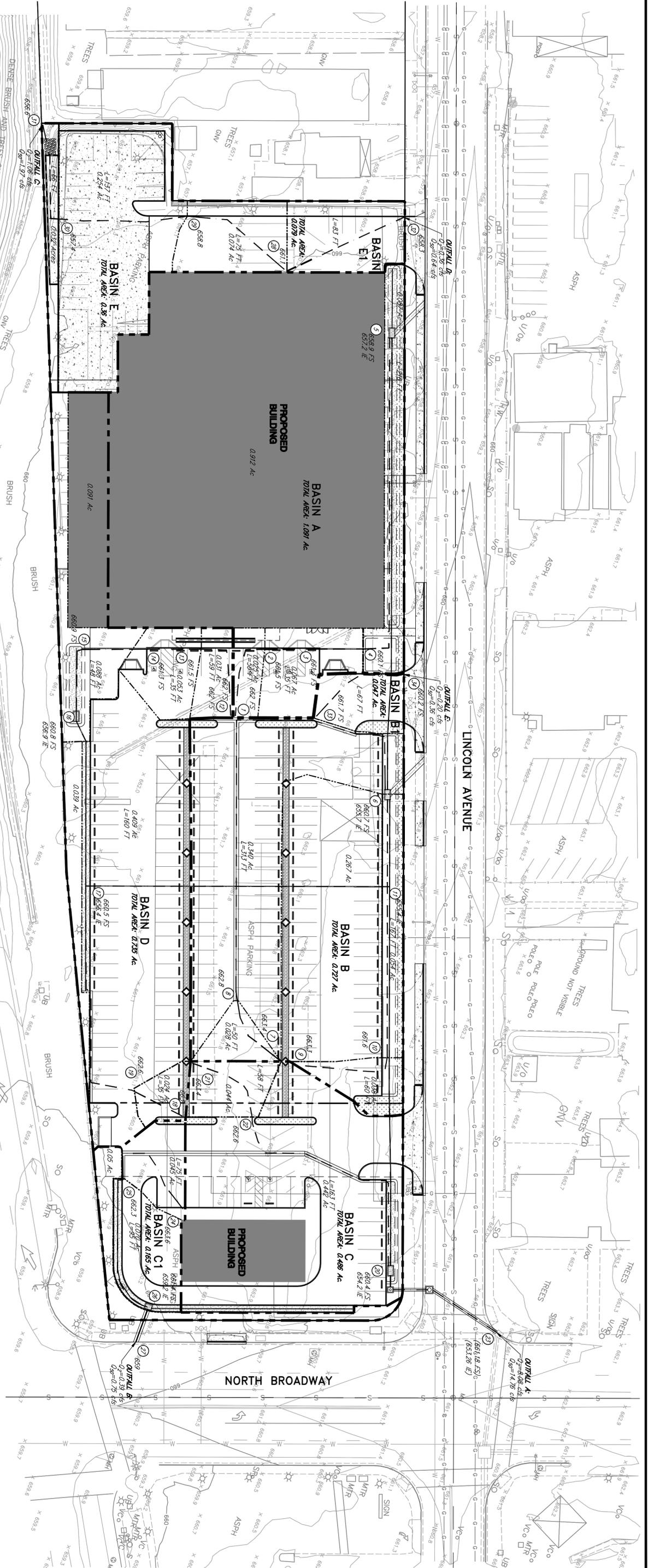


SCALE: 1"=30'
 0 30 60 90 120

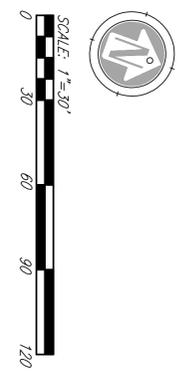
LEGEND - ABBREVIATIONS:
 - - - - - INDICATES TRIBUTARY AREA BOUNDARY.
 - - - - - INDICATES SUB TRIBUTARY AREA BOUNDARY
 - - - - - FLOW LINE
 L=66 FT FLOW DISTANCE

**GATEWAY CENTER
 HYDROLOGY PRE-DEVELOPMENT MAP**
 APN 229-121-08, 09, 10, 11,
 12, 13, 14, 15
 SITE ADDRESS: 990 NORTH BROADWAY
 ESCONDIDO, CA 92026





- LEGEND - ABBREVIATIONS:**
- INDICATES TRIBUTARY AREA BOUNDARY.
 - INDICATES SUB TRIBUTARY AREA BOUNDARY
 - FLOW LINE
 - L=66 FT SUB BASIN AREA (AGRES)
 - 1.234 Ac
 - 660.7
 - ⑦ NODE AND ELEVATION



**CENTERPOINTE 78
HYDROLOGY POST-DEVELOPMENT MAP**

APN 229-121-08, 09, 10, 11,
12, 13, 14, 15

SITE ADDRESS: 990 NORTH BROADWAY
ESCONDIDO, CA 92026



ATTACHMENT E
PRE/POST DEVELOPMENT HYDROLOGIC
2 YEAR & 50 YEAR 6 HR STORM ANALYSES

PRE-DEVELOPMENT

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software, (c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/25/13

***** Hydrology Study Control Information *****
BASIN A - OUTFALL A

Program License Serial Number 4012

Rational hydrology study storm event year is 2.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 1.550
24 hour precipitation(inches) = 2.400
P6/P24 = 64.6%
San Diego hydrology manual 'C' values used

Process from Point/Station 1.000 to Point/Station 2.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(Office Professional)
Impervious value, Ai = 0.900
Sub-Area C Value = 0.850
Initial subarea total flow distance = 57.000(Ft.)
Highest elevation = 663.500(Ft.)
Lowest elevation = 662.800(Ft.)
Elevation difference = 0.700(Ft.) Slope = 1.228 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 60.00 (Ft)
for the top area slope value of 1.23 %, in a development type of
Office Professional
In Accordance With Figure 3-3
Initial Area Time of Concentration = 3.26 minutes
TC = $[1.8 * (1.1 - C) * \text{distance}(\text{Ft.})^{.5} / (\% \text{ slope}^{1/3})]$
TC = $[1.8 * (1.1 - 0.8500) * (60.000^{.5}) / (1.228^{1/3})] = 3.26$
Rainfall intensity (I) = 5.386(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.850
Subarea runoff = 0.760(CFS)
Total initial stream area = 0.166(Ac.)

Process from Point/Station 2.000 to Point/Station 3.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 2.161(CFS)
Depth of flow = 0.141(Ft.), Average velocity = 1.704(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 0.60
2 40.00 0.00
3 70.00 0.50

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software, (c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/25/13

***** Hydrology Study Control Information *****
BASIN A - OUTFALL A

Program License Serial Number 4012

Rational hydrology study storm event year is 50.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 2.750
24 hour precipitation(inches) = 5.750
P6/P24 = 47.8%
San Diego hydrology manual 'C' values used

+++++
Process from Point/Station 1.000 to Point/Station 2.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(Office Professional)
Impervious value, Ai = 0.900
Sub-Area C Value = 0.850
Initial subarea total flow distance = 57.000(Ft.)
Highest elevation = 663.500(Ft.)
Lowest elevation = 662.800(Ft.)
Elevation difference = 0.700(Ft.) Slope = 1.228 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 60.00 (Ft)
for the top area slope value of 1.23 %, in a development type of
Office Professional
In Accordance With Figure 3-3
Initial Area Time of Concentration = 3.26 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^{0.5}/(% slope^{1/3})]
TC = [1.8*(1.1-0.8500)*(60.000^{0.5})/(1.228^{1/3})] = 3.26
Rainfall intensity (I) = 9.557(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.850
Subarea runoff = 1.348(CFS)
Total initial stream area = 0.166(Ac.)

+++++
Process from Point/Station 2.000 to Point/Station 3.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 3.955(CFS)
Depth of flow = 0.177(Ft.), Average velocity = 1.983(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 0.60
2 40.00 0.00
3 70.00 0.50

Manning's 'N' friction factor = 0.013

Sub-Channel flow = 3.955(CFS)
' ' flow top width = 22.481(Ft.)
' ' velocity= 1.983(Ft/s)
' ' area = 1.995(Sq.Ft)
' ' Froude number = 1.173

Upstream point elevation = 662.800(Ft.)
Downstream point elevation = 659.600(Ft.)
Flow length = 421.000(Ft.)
Travel time = 3.54 min.
Time of concentration = 6.79 min.
Depth of flow = 0.177(Ft.)
Average velocity = 1.983(Ft/s)
Total irregular channel flow = 3.955(CFS)
Irregular channel normal depth above invert elev. = 0.177(Ft.)
Average velocity of channel(s) = 1.983(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(Office Professional)
Impervious value, Ai = 0.900
Sub-Area C Value = 0.850
Rainfall intensity = 5.945(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.850 CA = 1.090
Subarea runoff = 5.130(CFS) for 1.116(Ac.)
Total runoff = 6.479(CFS) Total area = 1.282(Ac.)
Depth of flow = 0.214(Ft.), Average velocity = 2.243(Ft/s)

+++++
Process from Point/Station 3.000 to Point/Station 3.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(Office Professional)
Impervious value, Ai = 0.900
Sub-Area C Value = 0.850
Time of concentration = 6.79 min.
Rainfall intensity = 5.945(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.850 CA = 1.433
Subarea runoff = 2.042(CFS) for 0.404(Ac.)
Total runoff = 8.520(CFS) Total area = 1.686(Ac.)
End of computations, total study area = 1.686 (Ac.)

Manning's 'N' friction factor = 0.013

Sub-Channel flow = 2.161(CFS)
' ' flow top width = 17.920(Ft.)
' ' velocity= 1.704(Ft/s)
' ' area = 1.268(Sq.Ft)
' ' Froude number = 1.129

Upstream point elevation = 662.800(Ft.)
Downstream point elevation = 659.600(Ft.)
Flow length = 421.000(Ft.)
Travel time = 4.12 min.
Time of concentration = 7.37 min.
Depth of flow = 0.141(Ft.)
Average velocity = 1.704(Ft/s)
Total irregular channel flow = 2.161(CFS)
Irregular channel normal depth above invert elev. = 0.141(Ft.)
Average velocity of channel(s) = 1.704(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(Office Professional)
Impervious value, Ai = 0.900
Sub-Area C Value = 0.850
Rainfall intensity = 3.179(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.850 CA = 1.090
Subarea runoff = 2.704(CFS) for 1.116(Ac.)
Total runoff = 3.464(CFS) Total area = 1.282(Ac.)
Depth of flow = 0.169(Ft.), Average velocity = 1.918(Ft/s)

+++++
Process from Point/Station 3.000 to Point/Station 3.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(Office Professional)
Impervious value, Ai = 0.900
Sub-Area C Value = 0.850
Time of concentration = 7.37 min.
Rainfall intensity = 3.179(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.850 CA = 1.433
Subarea runoff = 1.092(CFS) for 0.404(Ac.)
Total runoff = 4.556(CFS) Total area = 1.686(Ac.)
End of computations, total study area = 1.686 (Ac.)

San Diego County Rational Hydrology Program

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Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/20/13

***** Hydrology Study Control Information *****
BASIN B - OUTFALL B

Program License Serial Number 4012

Rational hydrology study storm event year is 2.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 1.550
24 hour precipitation(inches) = 2.400
P6/P24 = 64.6%
San Diego hydrology manual 'C' values used

+++++
Process from Point/Station 4.000 to Point/Station 5.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(Office Professional)
Impervious value, Ai = 0.900
Sub-Area C Value = 0.850
Initial subarea total flow distance = 60.000(Ft.)
Highest elevation = 661.000(Ft.)
Lowest elevation = 660.300(Ft.)
Elevation difference = 0.700(Ft.) Slope = 1.167 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 60.00 (Ft)
for the top area slope value of 1.17 %, in a development type of
Office Professional
In Accordance With Figure 3-3
Initial Area Time of Concentration = 3.31 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.8500)*(60.000^0.5)/(1.167^(1/3))]= 3.31
Rainfall intensity (I) = 5.328(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.850
Subarea runoff = 0.344(CFS)
Total initial stream area = 0.076(Ac.)

+++++
Process from Point/Station 5.000 to Point/Station 6.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 1.241(CFS)
Depth of flow = 0.165(Ft.), Average velocity = 1.682(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 0.40
2 12.00 0.00
3 24.00 0.50

Manning's 'N' friction factor = 0.013

Sub-Channel flow = 1.241(CFS)
' ' flow top width = 8.928(Ft.)
' ' velocity = 1.682(Ft/s)
' ' area = 0.738(Sq.Ft)
' ' Froude number = 1.031

Upstream point elevation = 660.300(Ft.)
Downstream point elevation = 659.000(Ft.)
Flow length = 216.000(Ft.)
Travel time = 2.14 min.
Time of concentration = 5.45 min.
Depth of flow = 0.165(Ft.)
Average velocity = 1.682(Ft/s)
Total irregular channel flow = 1.241(CFS)
Irregular channel normal depth above invert elev. = 0.165(Ft.)
Average velocity of channel(s) = 1.682(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(Office Professional)
Impervious value, Ai = 0.900
Sub-Area C Value = 0.850
Rainfall intensity = 3.863(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.850 CA = 0.539
Subarea runoff = 1.737(CFS) for 0.558(Ac.)
Total runoff = 2.082(CFS) Total area = 0.634(Ac.)
Depth of flow = 0.201(Ft.), Average velocity = 1.914(Ft/s)
End of computations, total study area = 0.634 (Ac.)

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software, (c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/20/13

***** Hydrology Study Control Information *****
BASIN B - OUTFALL B

Program License Serial Number 4012

Rational hydrology study storm event year is 50.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 2.750
24 hour precipitation(inches) = 5.750
P6/P24 = 47.8%
San Diego hydrology manual 'C' values used

+++++
Process from Point/Station 4.000 to Point/Station 5.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(Office Professional)
Impervious value, Ai = 0.900
Sub-Area C Value = 0.850
Initial subarea total flow distance = 60.000(Ft.)
Highest elevation = 661.000(Ft.)
Lowest elevation = 660.300(Ft.)
Elevation difference = 0.700(Ft.) Slope = 1.167 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 60.00 (Ft)
for the top area slope value of 1.17 %, in a development type of
Office Professional
In Accordance With Figure 3-3
Initial Area Time of Concentration = 3.31 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.8500)*(60.000^0.5)/(1.167^(1/3))]= 3.31
Rainfall intensity (I) = 9.453(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.850
Subarea runoff = 0.611(CFS)
Total initial stream area = 0.076(Ac.)

+++++
Process from Point/Station 5.000 to Point/Station 6.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 2.265(CFS)
Depth of flow = 0.207(Ft.), Average velocity = 1.955(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 0.40
2 12.00 0.00
3 24.00 0.50

Manning's 'N' friction factor = 0.013

Sub-Channel flow = 2.265(CFS)
' ' flow top width = 11.187(Ft.)
' ' velocity = 1.955(Ft/s)
' ' area = 1.159(Sq.Ft)
' ' Froude number = 1.070

Upstream point elevation = 660.300(Ft.)
Downstream point elevation = 659.000(Ft.)
Flow length = 216.000(Ft.)
Travel time = 1.84 min.
Time of concentration = 5.15 min.
Depth of flow = 0.207(Ft.)
Average velocity = 1.955(Ft/s)
Total irregular channel flow = 2.265(CFS)
Irregular channel normal depth above invert elev. = 0.207(Ft.)
Average velocity of channel(s) = 1.955(Ft/s)

Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(Office Professional)
Impervious value, Ai = 0.900
Sub-Area C Value = 0.850
Rainfall intensity = 7.107(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.850 CA = 0.539
Subarea runoff = 3.219(CFS) for 0.558(Ac.)
Total runoff = 3.830(CFS) Total area = 0.634(Ac.)
Depth of flow = 0.252(Ft.), Average velocity = 2.229(Ft/s)
End of computations, total study area = 0.634 (Ac.)

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software, (c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/20/13

***** Hydrology Study Control Information *****
BASIN C - OUTFALL C

Program License Serial Number 4012

Rational hydrology study storm event year is 2.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 1.550
24 hour precipitation(inches) = 2.400
P6/P24 = 64.6%
San Diego hydrology manual 'C' values used

+++++
Process from Point/Station 7.000 to Point/Station 8.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(Office Professional)
Impervious value, Ai = 0.900
Sub-Area C Value = 0.850
Initial subarea total flow distance = 60.000(Ft.)
Highest elevation = 662.200(Ft.)
Lowest elevation = 661.300(Ft.)
Elevation difference = 0.900(Ft.) Slope = 1.500 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 70.00 (Ft)
for the top area slope value of 1.50 %, in a development type of
Office Professional
In Accordance With Figure 3-3
Initial Area Time of Concentration = 3.29 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.8500)*(70.000^0.5)/(1.500^(1/3))]= 3.29
Rainfall intensity (I) = 5.351(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.850
Subarea runoff = 0.373(CFS)
Total initial stream area = 0.082(Ac.)

+++++
Process from Point/Station 8.000 to Point/Station 9.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 1.255(CFS)
Depth of flow = 0.111(Ft.), Average velocity = 1.705(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 0.50
2 30.00 0.00
3 60.00 0.50

Manning's 'N' friction factor = 0.013

Sub-Channel flow = 1.255(CFS)
' ' flow top width = 13.292(Ft.)
' ' velocity= 1.705(Ft/s)
' ' area = 0.736(Sq.Ft)
' ' Froude number = 1.277

Upstream point elevation = 661.300(Ft.)
Downstream point elevation = 658.600(Ft.)
Flow length = 256.000(Ft.)
Travel time = 2.50 min.
Time of concentration = 5.79 min.
Depth of flow = 0.111(Ft.)
Average velocity = 1.705(Ft/s)
Total irregular channel flow = 1.255(CFS)
Irregular channel normal depth above invert elev. = 0.111(Ft.)
Average velocity of channel(s) = 1.705(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(Office Professional)
Impervious value, Ai = 0.900
Sub-Area C Value = 0.850
Rainfall intensity = 3.715(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.850 CA = 0.558
Subarea runoff = 1.698(CFS) for 0.574(Ac.)
Total runoff = 2.071(CFS) Total area = 0.656(Ac.)
Depth of flow = 0.134(Ft.), Average velocity = 1.933(Ft/s)
End of computations, total study area = 0.656 (Ac.)

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software, (c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/20/13

***** Hydrology Study Control Information *****
BASIN C - OUTFALL C

Program License Serial Number 4012

Rational hydrology study storm event year is 50.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 2.750
24 hour precipitation(inches) = 5.750
P6/P24 = 47.8%
San Diego hydrology manual 'C' values used

+++++
Process from Point/Station 7.000 to Point/Station 8.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(Office Professional)
Impervious value, Ai = 0.900
Sub-Area C Value = 0.850
Initial subarea total flow distance = 60.000(Ft.)
Highest elevation = 662.200(Ft.)
Lowest elevation = 661.300(Ft.)
Elevation difference = 0.900(Ft.) Slope = 1.500 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 70.00 (Ft)
for the top area slope value of 1.50 %, in a development type of
Office Professional
In Accordance With Figure 3-3
Initial Area Time of Concentration = 3.29 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^{0.5}/(% slope^{1/3})]
TC = [1.8*(1.1-0.8500)*(70.000^{0.5})/(1.500^{1/3})] = 3.29
Rainfall intensity (I) = 9.493(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.850
Subarea runoff = 0.662(CFS)
Total initial stream area = 0.082(Ac.)

+++++
Process from Point/Station 8.000 to Point/Station 9.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 2.270(CFS)
Depth of flow = 0.138(Ft.), Average velocity = 1.978(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 0.50
2 30.00 0.00
3 60.00 0.50

Manning's 'N' friction factor = 0.013

Sub-Channel flow = 2.270(CFS)
' ' flow top width = 16.599(Ft.)
' ' velocity = 1.978(Ft/s)
' ' area = 1.148(Sq.Ft)
' ' Froude number = 1.325

Upstream point elevation = 661.300(Ft.)
Downstream point elevation = 658.600(Ft.)
Flow length = 256.000(Ft.)
Travel time = 2.16 min.
Time of concentration = 5.45 min.
Depth of flow = 0.138(Ft.)
Average velocity = 1.978(Ft/s)
Total irregular channel flow = 2.270(CFS)
Irregular channel normal depth above invert elev. = 0.138(Ft.)
Average velocity of channel(s) = 1.978(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(Office Professional)
Impervious value, Ai = 0.900
Sub-Area C Value = 0.850
Rainfall intensity = 6.857(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.850 CA = 0.558
Subarea runoff = 3.162(CFS) for 0.574(Ac.)
Total runoff = 3.823(CFS) Total area = 0.656(Ac.)
Depth of flow = 0.168(Ft.), Average velocity = 2.253(Ft/s)
End of computations, total study area = 0.656 (Ac.)

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software, (c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/20/13

***** Hydrology Study Control Information *****
BASIN D - OUTFALL D

Program License Serial Number 4012

Rational hydrology study storm event year is 2.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 1.550
24 hour precipitation(inches) = 2.400
P6/P24 = 64.6%
San Diego hydrology manual 'C' values used

+++++
Process from Point/Station 10.000 to Point/Station 11.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(Office Professional)
Impervious value, Ai = 0.900
Sub-Area C Value = 0.850
Initial subarea total flow distance = 40.000(Ft.)
Highest elevation = 662.900(Ft.)
Lowest elevation = 661.000(Ft.)
Elevation difference = 1.900(Ft.) Slope = 4.750 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 90.00 (Ft)
for the top area slope value of 4.75 %, in a development type of
Office Professional
In Accordance With Figure 3-3
Initial Area Time of Concentration = 2.54 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^{0.5}/(% slope^{1/3})]
TC = [1.8*(1.1-0.8500)*(90.000^{0.5})/(4.750^{1/3})] = 2.54
Rainfall intensity (I) = 6.322(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.850
Subarea runoff = 0.355(CFS)
Total initial stream area = 0.066(Ac.)

+++++
Process from Point/Station 11.000 to Point/Station 12.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.950(CFS)
Depth of flow = 0.061(Ft.), Average velocity = 1.707(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 0.20
2 30.00 0.00
3 60.00 0.20

Manning's 'N' friction factor = 0.013

Sub-Channel flow = 0.950(CFS)
' ' flow top width = 18.277(Ft.)
' ' velocity = 1.707(Ft/s)
' ' area = 0.557(Sq.Ft)
' ' Froude number = 1.723

Upstream point elevation = 661.000(Ft.)
Downstream point elevation = 659.500(Ft.)
Flow length = 64.000(Ft.)
Travel time = 0.62 min.
Time of concentration = 3.16 min.
Depth of flow = 0.061(Ft.)
Average velocity = 1.707(Ft/s)
Total irregular channel flow = 0.950(CFS)
Irregular channel normal depth above invert elev. = 0.061(Ft.)
Average velocity of channel(s) = 1.707(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(Office Professional)
Impervious value, Ai = 0.900
Sub-Area C Value = 0.850
Rainfall intensity = 5.485(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.850 CA = 0.271
Subarea runoff = 1.133(CFS) for 0.253(Ac.)
Total runoff = 1.487(CFS) Total area = 0.319(Ac.)
Depth of flow = 0.072(Ft.), Average velocity = 1.909(Ft/s)
End of computations, total study area = 0.319 (Ac.)

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software, (c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/20/13

***** Hydrology Study Control Information *****
BASIN D - OUTFALL D

Program License Serial Number 4012

Rational hydrology study storm event year is 50.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 2.750
24 hour precipitation(inches) = 5.750
P6/P24 = 47.8%
San Diego hydrology manual 'C' values used

+++++
Process from Point/Station 10.000 to Point/Station 11.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(Office Professional)
Impervious value, Ai = 0.900
Sub-Area C Value = 0.850
Initial subarea total flow distance = 40.000(Ft.)
Highest elevation = 662.900(Ft.)
Lowest elevation = 661.000(Ft.)
Elevation difference = 1.900(Ft.) Slope = 4.750 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 90.00 (Ft)
for the top area slope value of 4.75 %, in a development type of
Office Professional
In Accordance With Figure 3-3
Initial Area Time of Concentration = 2.54 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.8500)*(90.000^0.5)/(4.750^(1/3))]= 2.54
Rainfall intensity (I) = 11.216(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.850
Subarea runoff = 0.629(CFS)
Total initial stream area = 0.066(Ac.)

+++++
Process from Point/Station 11.000 to Point/Station 12.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 1.703(CFS)
Depth of flow = 0.076(Ft.), Average velocity = 1.975(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 0.20
2 30.00 0.00
3 60.00 0.20

Manning's 'N' friction factor = 0.013

Sub-Channel flow = 1.703(CFS)
' ' flow top width = 22.747(Ft.)
' ' velocity = 1.975(Ft/s)
' ' area = 0.862(Sq.Ft)
' ' Froude number = 1.787

Upstream point elevation = 661.000(Ft.)
Downstream point elevation = 659.500(Ft.)
Flow length = 64.000(Ft.)
Travel time = 0.54 min.
Time of concentration = 3.08 min.
Depth of flow = 0.076(Ft.)
Average velocity = 1.975(Ft/s)
Total irregular channel flow = 1.703(CFS)
Irregular channel normal depth above invert elev. = 0.076(Ft.)
Average velocity of channel(s) = 1.975(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(Office Professional)
Impervious value, Ai = 0.900
Sub-Area C Value = 0.850
Rainfall intensity = 9.904(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.850 CA = 0.271
Subarea runoff = 2.056(CFS) for 0.253(Ac.)
Total runoff = 2.685(CFS) Total area = 0.319(Ac.)
Depth of flow = 0.090(Ft.), Average velocity = 2.213(Ft/s)
End of computations, total study area = 0.319 (Ac.)

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software, (c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/20/13

***** Hydrology Study Control Information *****
BASIN E - OUTFALL E

Program License Serial Number 4012

Rational hydrology study storm event year is 2.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 1.550
24 hour precipitation(inches) = 2.400
P6/P24 = 64.6%
San Diego hydrology manual 'C' values used

+-----+
Process from Point/Station 13.000 to Point/Station 14.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(Office Professional)
Impervious value, Ai = 0.900
Sub-Area C Value = 0.850
Initial subarea total flow distance = 55.000(Ft.)
Highest elevation = 661.700(Ft.)
Lowest elevation = 660.700(Ft.)
Elevation difference = 1.000(Ft.) Slope = 1.818 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 70.00 (Ft)
for the top area slope value of 1.82 %, in a development type of
Office Professional
In Accordance With Figure 3-3
Initial Area Time of Concentration = 3.08 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.8500)*(70.000^0.5)/(1.818^(1/3))]= 3.08
Rainfall intensity (I) = 5.576(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.850
Subarea runoff = 0.337(CFS)
Total initial stream area = 0.071(Ac.)

+-----+
Process from Point/Station 14.000 to Point/Station 14.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(Office Professional)
Impervious value, Ai = 0.900
Sub-Area C Value = 0.850
Time of concentration = 3.08 min.

Rainfall intensity = 5.576(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.850 CA = 0.291
Subarea runoff = 1.285(CFS) for 0.271(Ac.)
Total runoff = 1.621(CFS) Total area = 0.342(Ac.)
End of computations, total study area = 0.342 (Ac.)

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software, (c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/20/13

***** Hydrology Study Control Information *****
BASIN E - OUTFALL E

Program License Serial Number 4012

Rational hydrology study storm event year is 50.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 2.750
24 hour precipitation(inches) = 5.750
P6/P24 = 47.8%
San Diego hydrology manual 'C' values used

+++++
Process from Point/Station 13.000 to Point/Station 14.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(Office Professional)
Impervious value, Ai = 0.900
Sub-Area C Value = 0.850
Initial subarea total flow distance = 55.000(Ft.)
Highest elevation = 661.700(Ft.)
Lowest elevation = 660.700(Ft.)
Elevation difference = 1.000(Ft.) Slope = 1.818 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 70.00 (Ft)
for the top area slope value of 1.82 %, in a development type of
Office Professional
In Accordance With Figure 3-3
Initial Area Time of Concentration = 3.08 minutes
TC = $[1.8 * (1.1 - C) * \text{distance}(\text{Ft.})^{.5} / (\% \text{ slope}^{(1/3)})]$
TC = $[1.8 * (1.1 - 0.8500) * (70.000^{.5}) / (1.818^{(1/3)})] = 3.08$
Rainfall intensity (I) = 9.894(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.850
Subarea runoff = 0.597(CFS)
Total initial stream area = 0.071(Ac.)

+++++
Process from Point/Station 14.000 to Point/Station 14.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(Office Professional)
Impervious value, Ai = 0.900
Sub-Area C Value = 0.850
Time of concentration = 3.08 min.

Rainfall intensity = 9.894(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.850 CA = 0.291
Subarea runoff = 2.279(CFS) for 0.271(Ac.)
Total runoff = 2.876(CFS) Total area = 0.342(Ac.)
End of computations, total study area = 0.342 (Ac.)

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software, (c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/20/13

***** Hydrology Study Control Information *****
BASIN F - OUTFALL F

Program License Serial Number 4012

Rational hydrology study storm event year is 2.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 1.550
24 hour precipitation(inches) = 2.400
P6/P24 = 64.6%
San Diego hydrology manual 'C' values used

+++++
Process from Point/Station 15.000 to Point/Station 16.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN]
(Permanent Open Space)
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Initial subarea total flow distance = 79.000(Ft.)
Highest elevation = 658.500(Ft.)
Lowest elevation = 655.900(Ft.)
Elevation difference = 2.600(Ft.) Slope = 3.291 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 3.29 %, in a development type of
Permanent Open Space
In Accordance With Figure 3-3
Initial Area Time of Concentration = 9.08 minutes
TC = $[1.8 * (1.1 - C) * \text{distance}(\text{Ft.})^{0.5} / (\% \text{ slope}^{1/3})]$
TC = $[1.8 * (1.1 - 0.3500) * (100.000^{0.5}) / (3.291^{1/3})] = 9.08$
Rainfall intensity (I) = 2.780(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.350
Subarea runoff = 0.021(CFS)
Total initial stream area = 0.022(Ac.)

+++++
Process from Point/Station 16.000 to Point/Station 16.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN]
(Permanent Open Space)
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Time of concentration = 9.08 min.

Rainfall intensity = 2.780(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for total area
($Q=KCIA$) is $C = 0.350$ $CA = 0.019$
Subarea runoff = 0.031(CFS) for 0.032(Ac.)
Total runoff = 0.053(CFS) Total area = 0.054(Ac.)
End of computations, total study area = 0.054 (Ac.)

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software, (c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 02/20/13

***** Hydrology Study Control Information *****
BASIN F - OUTFALL F

Program License Serial Number 4012

Rational hydrology study storm event year is 50.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 2.750
24 hour precipitation(inches) = 5.750
P6/P24 = 47.8%
San Diego hydrology manual 'C' values used

Process from Point/Station 15.000 to Point/Station 16.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN]
(Permanent Open Space)
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Initial subarea total flow distance = 79.000(Ft.)
Highest elevation = 658.500(Ft.)
Lowest elevation = 655.900(Ft.)
Elevation difference = 2.600(Ft.) Slope = 3.291 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 100.00 (Ft)
for the top area slope value of 3.29 %, in a development type of
Permanent Open Space
In Accordance With Figure 3-3
Initial Area Time of Concentration = 9.08 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^{0.5}/(% slope^{1/3})]
TC = [1.8*(1.1-0.3500)*(100.000^{0.5})/(3.291^{1/3})] = 9.08
Rainfall intensity (I) = 4.932(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.350
Subarea runoff = 0.038(CFS)
Total initial stream area = 0.022(Ac.)

Process from Point/Station 16.000 to Point/Station 16.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[UNDISTURBED NATURAL TERRAIN]
(Permanent Open Space)
Impervious value, Ai = 0.000
Sub-Area C Value = 0.350
Time of concentration = 9.08 min.

Rainfall intensity = 4.932(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.350 CA = 0.019
Subarea runoff = 0.055(CFS) for 0.032(Ac.)
Total runoff = 0.093(CFS) Total area = 0.054(Ac.)
End of computations, total study area = 0.054 (Ac.)

POST-DEVELOPMENT

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 04/02/13

Outfall A
Basin A, B, C, and D
2 Year Rainfall Event

***** Hydrology Study Control Information *****

Program License Serial Number 4012

Rational hydrology study storm event year is 2.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 1.550
24 hour precipitation(inches) = 2.400
P6/P24 = 64.6%
San Diego hydrology manual 'C' values used

Process from Point/Station 1.000 to Point/Station 2.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Initial subarea total flow distance = 56.000(Ft.)
Highest elevation = 662.000(Ft.)
Lowest elevation = 661.500(Ft.)
Elevation difference = 0.500(Ft.) Slope = 0.893 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 60.00 (Ft)
for the top area slope value of 0.89 %, in a development type of
General Commercial
In Accordance With Figure 3-3
Initial Area Time of Concentration = 4.05 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.8200)*(60.000^0.5)]/(0.893^(1/3))= 4.05
Rainfall intensity (I) = 4.675(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.820
Subarea runoff = 0.096(CFS)
Total initial stream area = 0.025(Ac.)

Process from Point/Station 2.000 to Point/Station 3.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.224(CFS)
Depth of flow = 0.070(Ft.), Average velocity = 0.918(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :

Point number 'X' coordinate 'Y' coordinate
1 0.00 0.45
2 45.00 0.00
3 45.50 0.50

Manning's 'N' friction factor = 0.013

Sub-Channel flow = 0.224(CFS)
' ' flow top width = 7.025(Ft.)
' ' velocity = 0.918(Ft/s)
' ' area = 0.244(Sq.Ft)
' ' Froude number = 0.868

Upstream point elevation = 661.500(Ft.)
Downstream point elevation = 661.300(Ft.)
Flow length = 35.000(Ft.)
Travel time = 0.64 min.
Time of concentration = 4.69 min.
Depth of flow = 0.070(Ft.)
Average velocity = 0.918(Ft/s)
Total irregular channel flow = 0.224(CFS)
Irregular channel normal depth above invert elev. = 0.070(Ft.)
Average velocity of channel(s) = 0.918(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Rainfall intensity = 4.256(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.820 CA = 0.075
Subarea runoff = 0.225(CFS) for 0.067(Ac.)
Total runoff = 0.321(CFS) Total area = 0.092(Ac.)
Depth of flow = 0.080(Ft.), Average velocity = 1.004(Ft/s)

Process from Point/Station 3.000 to Point/Station 4.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 661.300(Ft.)
Downstream point/station elevation = 660.100(Ft.)
Pipe length = 30.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.321(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.321(CFS)
Normal flow depth in pipe = 2.20(In.)
Flow top width inside pipe = 5.78(In.)
Critical Depth = 3.45(In.)
Pipe flow velocity = 4.93(Ft/s)
Travel time through pipe = 0.10 min.
Time of concentration (TC) = 4.79 min.

Process from Point/Station 4.000 to Point/Station 4.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Time of concentration = 4.79 min.
Rainfall intensity = 4.198(In/Hr) for a 2.0 year storm

Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.820 CA = 0.823
Subarea runoff = 3.135(CFS) for 0.912(Ac.)
Total runoff = 3.456(CFS) Total area = 1.004(Ac.)

Process from Point/Station 4.000 to Point/Station 5.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 3.494(CFS)
Depth of flow = 0.324(Ft.), Average velocity = 1.544(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 0.53
2 2.10 0.00
3 7.80 0.00
4 9.90 0.53
Manning's 'N' friction factor = 0.030

Sub-Channel flow = 3.494(CFS)
' ' flow top width = 8.288(Ft.)
' ' velocity = 1.544(Ft/s)
' ' area = 2.263(Sq.Ft)
' ' Froude number = 0.521

Upstream point elevation = 660.100(Ft.)
Downstream point elevation = 658.900(Ft.)
Flow length = 216.000(Ft.)
Travel time = 2.33 min.
Time of concentration = 7.12 min.
Depth of flow = 0.324(Ft.)
Average velocity = 1.544(Ft/s)
Total irregular channel flow = 3.494(CFS)
Irregular channel normal depth above invert elev. = 0.324(Ft.)
Average velocity of channel(s) = 1.544(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]

(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
The area added to the existing stream causes a
a lower flow rate of Q = 2.908(CFS)
therefore the upstream flow rate of Q = 3.456(CFS) is being used
Rainfall intensity = 3.251(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.820 CA = 0.895
Subarea runoff = 0.000(CFS) for 0.087(Ac.)
Total runoff = 3.456(CFS) Total area = 1.091(Ac.)
Depth of flow = 0.322(Ft.), Average velocity = 1.538(Ft/s)

Process from Point/Station 5.000 to Point/Station 6.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 657.200(Ft.)
Downstream point/station elevation = 655.700(Ft.)
Pipe length = 293.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 3.456(CFS)
Nearest computed pipe diameter = 15.00(In.)
Calculated individual pipe flow = 3.456(CFS)
Normal flow depth in pipe = 9.67(In.)
Flow top width inside pipe = 14.36(In.)
Critical Depth = 9.00(In.)

Pipe flow velocity = 4.13(Ft/s)
Travel time through pipe = 1.18 min.
Time of concentration (TC) = 8.30 min.

Process from Point/Station 6.000 to Point/Station 6.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 1.091(Ac.)
Runoff from this stream = 3.456(CFS)
Time of concentration = 8.30 min.
Rainfall intensity = 2.944(In/Hr)

Process from Point/Station 7.000 to Point/Station 8.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Initial subarea total flow distance = 50.000(Ft.)
Highest elevation = 663.400(Ft.)
Lowest elevation = 662.800(Ft.)
Elevation difference = 0.600(Ft.) Slope = 1.200 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 60.00 (Ft)
for the top area slope value of 1.20 %, in a development type of
General Commercial
In Accordance With Figure 3-3
Initial Area Time of Concentration = 3.67 minutes
TC = $[1.8*(1.1-C)*distance(Ft.)^{.5}]/(%\ slope^{(1/3)})]$
TC = $[1.8*(1.1-0.8200)*(60.000^{.5})/(1.200^{(1/3)})]= 3.67$
Rainfall intensity (I) = 4.982(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.820
Subarea runoff = 0.114(CFS)
Total initial stream area = 0.028(Ac.)

Process from Point/Station 8.000 to Point/Station 6.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.538(CFS)
Depth of flow = 0.077(Ft.), Average velocity = 1.065(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 0.35
2 30.00 0.00
3 60.00 0.35
Manning's 'N' friction factor = 0.013

Sub-Channel flow = 0.538(CFS)
' ' flow top width = 13.155(Ft.)
' ' velocity= 1.065(Ft/s)
' ' area = 0.505(Sq.Ft)
' ' Froude number = 0.958

Upstream point elevation = 662.800(Ft.)
Downstream point elevation = 660.700(Ft.)
Flow length = 313.000(Ft.)
Travel time = 4.90 min.

Time of concentration = 8.57 min.
 Depth of flow = 0.077(Ft.)
 Average velocity = 1.065(Ft/s)
 Total irregular channel flow = 0.538(CFS)
 Irregular channel normal depth above invert elev. = 0.077(Ft.)
 Average velocity of channel(s) = 1.065(Ft/s)
 Adding area flow to channel
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [COMMERCIAL area type]
 (General Commercial)
 Impervious value, Ai = 0.850
 Sub-Area C Value = 0.820
 Rainfall intensity = 2.885(In/Hr) for a 2.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.820 CA = 0.302
 Subarea runoff = 0.756(CFS) for 0.340(Ac.)
 Total runoff = 0.870(CFS) Total area = 0.368(Ac.)
 Depth of flow = 0.092(Ft.), Average velocity = 1.201(Ft/s)

+-----+
 Process from Point/Station 6.000 to Point/Station 6.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.368(Ac.)
 Runoff from this stream = 0.870(CFS)
 Time of concentration = 8.57 min.
 Rainfall intensity = 2.885(In/Hr)

+-----+
 Process from Point/Station 9.000 to Point/Station 10.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [COMMERCIAL area type]
 (General Commercial)
 Impervious value, Ai = 0.850
 Sub-Area C Value = 0.820
 Initial subarea total flow distance = 60.000(Ft.)
 Highest elevation = 663.300(Ft.)
 Lowest elevation = 661.600(Ft.)
 Elevation difference = 1.700(Ft.) Slope = 2.833 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 85.00 (Ft)
 for the top area slope value of 2.83 %, in a development type of
 General Commercial
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 3.28 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{0.5}] / (\% slope^{(1/3)})$
 $TC = [1.8 * (1.1 - 0.8200) * (85.000^{0.5})] / (2.833^{(1/3)}) = 3.28$
 Rainfall intensity (I) = 5.356(In/Hr) for a 2.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.820
 Subarea runoff = 0.167(CFS)
 Total initial stream area = 0.038(Ac.)

+-----+
 Process from Point/Station 10.000 to Point/Station 10.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 1.000
 [COMMERCIAL area type]
 (General Commercial)
 Impervious value, Ai = 0.850
 Sub-Area C Value = 0.820
 Time of concentration = 3.28 min.
 Rainfall intensity = 5.356(In/Hr) for a 2.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.820 CA = 0.250
 Subarea runoff = 1.173(CFS) for 0.267(Ac.)
 Total runoff = 1.340(CFS) Total area = 0.305(Ac.)

 Process from Point/Station 10.000 to Point/Station 6.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

 Estimated mean flow rate at midpoint of channel = 1.369(CFS)
 Depth of flow = 0.155(Ft.), Average velocity = 1.020(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 0.50
 2 0.50 0.00
 3 8.83 0.00
 4 10.33 0.50
 Manning's 'N' friction factor = 0.030

Sub-Channel flow = 1.369(CFS)
 ' ' flow top width = 8.952(Ft.)
 ' ' velocity = 1.020(Ft/s)
 ' ' area = 1.343(Sq.Ft)
 ' ' Froude number = 0.464

Upstream point elevation = 661.600(Ft.)
 Downstream point elevation = 660.700(Ft.)
 Flow length = 167.000(Ft.)
 Travel time = 2.73 min.
 Time of concentration = 6.01 min.
 Depth of flow = 0.155(Ft.)
 Average velocity = 1.020(Ft/s)
 Total irregular channel flow = 1.369(CFS)
 Irregular channel normal depth above invert elev. = 0.155(Ft.)
 Average velocity of channel(s) = 1.020(Ft/s)
 Adding area flow to channel

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [COMMERCIAL area type]
 (General Commercial)

Impervious value, Ai = 0.850
 Sub-Area C Value = 0.820
 The area added to the existing stream causes a
 a lower flow rate of Q = 1.067(CFS)
 therefore the upstream flow rate of Q = 1.340(CFS) is being used
 Rainfall intensity = 3.626(In/Hr) for a 2.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.820 CA = 0.294
 Subarea runoff = 0.000(CFS) for 0.054(Ac.)
 Total runoff = 1.340(CFS) Total area = 0.359(Ac.)
 Depth of flow = 0.153(Ft.), Average velocity = 1.011(Ft/s)

 Process from Point/Station 6.000 to Point/Station 6.000
 **** CONFLUENCE OF MINOR STREAMS ****

 Along Main Stream number: 1 in normal stream number 3
 Stream flow area = 0.359(Ac.)

Runoff from this stream = 1.340(CFS)
 Time of concentration = 6.01 min.
 Rainfall intensity = 3.626(In/Hr)
 Summary of stream data:

| Stream No. | Flow rate (CFS) | TC (min) | Rainfall Intensity (In/Hr) |
|------------|-----------------|----------|----------------------------|
| 1 | 3.456 | 8.30 | 2.944 |
| 2 | 0.870 | 8.57 | 2.885 |
| 3 | 1.340 | 6.01 | 3.626 |

Qmax(1) =
 1.000 * 1.000 * 3.456) +
 1.000 * 0.969 * 0.870) +
 0.812 * 1.000 * 1.340) + = 5.387

Qmax(2) =
 0.980 * 1.000 * 3.456) +
 1.000 * 1.000 * 0.870) +
 0.796 * 1.000 * 1.340) + = 5.322

Qmax(3) =
 1.000 * 0.724 * 3.456) +
 1.000 * 0.702 * 0.870) +
 1.000 * 1.000 * 1.340) + = 4.453

Total of 3 streams to confluence:
 Flow rates before confluence point:
 3.456 0.870 1.340
 Maximum flow rates at confluence using above data:
 5.387 5.322 4.453
 Area of streams before confluence:
 1.091 0.368 0.359

Results of confluence:
 Total flow rate = 5.387(CFS)
 Time of concentration = 8.305 min.
 Effective stream area after confluence = 1.818(Ac.)

 Process from Point/Station 6.000 to Point/Station 11.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 655.700(Ft.)
 Downstream point/station elevation = 655.400(Ft.)
 Pipe length = 57.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 5.387(CFS)
 Nearest computed pipe diameter = 18.00(In.)
 Calculated individual pipe flow = 5.387(CFS)
 Normal flow depth in pipe = 11.17(In.)
 Flow top width inside pipe = 17.47(In.)
 Critical Depth = 10.73(In.)
 Pipe flow velocity = 4.68(Ft/s)
 Travel time through pipe = 0.20 min.
 Time of concentration (TC) = 8.51 min.

 Process from Point/Station 11.000 to Point/Station 11.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
 In Main Stream number: 1
 Stream flow area = 1.818(Ac.)
 Runoff from this stream = 5.387(CFS)
 Time of concentration = 8.51 min.
 Rainfall intensity = 2.898(In/Hr)
 Program is now starting with Main Stream No. 2

 Process from Point/Station 12.000 to Point/Station 13.000

**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Initial subarea total flow distance = 59.000(Ft.)
Highest elevation = 662.000(Ft.)
Lowest elevation = 661.500(Ft.)
Elevation difference = 0.500(Ft.) Slope = 0.847 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 60.00 (Ft)
for the top area slope value of 0.85 %, in a development type of
General Commercial
In Accordance With Figure 3-3
Initial Area Time of Concentration = 4.13 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.8200)*(60.000^0.5)/(0.847^(1/3))]= 4.13
Rainfall intensity (I) = 4.623(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.820
Subarea runoff = 0.118(CFS)
Total initial stream area = 0.031(Ac.)

Process from Point/Station 13.000 to Point/Station 14.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.218(CFS)
Depth of flow = 0.077(Ft.), Average velocity = 0.986(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 0.64
2 46.50 0.00
3 47.00 0.50
Manning's 'N' friction factor = 0.013

Sub-Channel flow = 0.218(CFS)
' ' flow top width = 5.708(Ft.)
' ' velocity= 0.986(Ft/s)
' ' area = 0.221(Sq.Ft)
' ' Froude number = 0.882

Upstream point elevation = 661.500(Ft.)
Downstream point elevation = 661.300(Ft.)
Flow length = 35.000(Ft.)
Travel time = 0.59 min.
Time of concentration = 4.72 min.
Depth of flow = 0.077(Ft.)
Average velocity = 0.986(Ft/s)
Total irregular channel flow = 0.218(CFS)
Irregular channel normal depth above invert elev. = 0.077(Ft.)
Average velocity of channel(s) = 0.986(Ft/s)

Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Rainfall intensity = 4.240(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.820 CA = 0.069

Subarea runoff = 0.175(CFS) for 0.053(Ac.)
Total runoff = 0.292(CFS) Total area = 0.084(Ac.)
Depth of flow = 0.086(Ft.), Average velocity = 1.060(Ft/s)

Process from Point/Station 14.000 to Point/Station 15.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 661.300(Ft.)
Downstream point/station elevation = 660.900(Ft.)
Pipe length = 42.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.292(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.292(CFS)
Normal flow depth in pipe = 3.12(In.)
Flow top width inside pipe = 6.00(In.)
Critical Depth = 3.28(In.)
Pipe flow velocity = 2.83(Ft/s)
Travel time through pipe = 0.25 min.
Time of concentration (TC) = 4.97 min.

Process from Point/Station 15.000 to Point/Station 15.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Time of concentration = 4.97 min.
Rainfall intensity = 4.102(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.820 CA = 0.143
Subarea runoff = 0.297(CFS) for 0.091(Ac.)
Total runoff = 0.589(CFS) Total area = 0.175(Ac.)

Process from Point/Station 15.000 to Point/Station 16.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.705(CFS)
Depth of flow = 0.141(Ft.), Average velocity = 0.585(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 0.50
2 2.00 0.00
3 10.00 0.00
4 12.00 0.50
Manning's 'N' friction factor = 0.030

Sub-Channel flow = 0.705(CFS)
' ' flow top width = 9.126(Ft.)
' ' velocity = 0.585(Ft/s)
' ' area = 1.205(Sq.Ft)
' ' Froude number = 0.284

Upstream point elevation = 660.900(Ft.)
Downstream point elevation = 660.800(Ft.)
Flow length = 48.000(Ft.)
Travel time = 1.37 min.
Time of concentration = 6.33 min.
Depth of flow = 0.141(Ft.)

Average velocity = 0.585(Ft/s)
Total irregular channel flow = 0.705(CFS)
Irregular channel normal depth above invert elev. = 0.141(Ft.)
Average velocity of channel(s) = 0.585(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Rainfall intensity = 3.506(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.820 CA = 0.216
Subarea runoff = 0.168(CFS) for 0.088(Ac.)
Total runoff = 0.756(CFS) Total area = 0.263(Ac.)
Depth of flow = 0.147(Ft.), Average velocity = 0.600(Ft/s)

Process from Point/Station 16.000 to Point/Station 17.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 656.900(Ft.)
Downstream point/station elevation = 656.400(Ft.)
Pipe length = 108.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.756(CFS)
Nearest computed pipe diameter = 9.00(In.)
Calculated individual pipe flow = 0.756(CFS)
Normal flow depth in pipe = 5.40(In.)
Flow top width inside pipe = 8.82(In.)
Critical Depth = 4.76(In.)
Pipe flow velocity = 2.73(Ft/s)
Travel time through pipe = 0.66 min.
Time of concentration (TC) = 6.99 min.

Process from Point/Station 17.000 to Point/Station 17.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Time of concentration = 6.99 min.
Rainfall intensity = 3.290(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.820 CA = 0.248
Subarea runoff = 0.058(CFS) for 0.039(Ac.)
Total runoff = 0.815(CFS) Total area = 0.302(Ac.)

Process from Point/Station 17.000 to Point/Station 17.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 1
Stream flow area = 0.302(Ac.)
Runoff from this stream = 0.815(CFS)
Time of concentration = 6.99 min.
Rainfall intensity = 3.290(In/Hr)

Process from Point/Station 18.000 to Point/Station 19.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Initial subarea total flow distance = 35.000(Ft.)
Highest elevation = 663.000(Ft.)
Lowest elevation = 662.600(Ft.)
Elevation difference = 0.400(Ft.) Slope = 1.143 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 60.00 (Ft)
for the top area slope value of 1.14 %, in a development type of
General Commercial
In Accordance With Figure 3-3
Initial Area Time of Concentration = 3.73 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.8200)*(60.000^0.5)/(1.143^(1/3))]= 3.73
Rainfall intensity (I) = 4.930(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for area (Q=K CIA) is C = 0.820
Subarea runoff = 0.097(CFS)
Total initial stream area = 0.024(Ac.)

Process from Point/Station 19.000 to Point/Station 17.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.814(CFS)
Depth of flow = 0.134(Ft.), Average velocity = 2.148(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 1.46
2 60.00 0.00
3 60.50 0.50
Manning's 'N' friction factor = 0.013

Sub-Channel flow = 0.814(CFS)
' ' flow top width = 5.650(Ft.)
' ' velocity = 2.148(Ft/s)
' ' area = 0.379(Sq.Ft)
' ' Froude number = 1.461

Upstream point elevation = 662.600(Ft.)
Downstream point elevation = 660.500(Ft.)
Flow length = 160.000(Ft.)
Travel time = 1.24 min.
Time of concentration = 4.98 min.
Depth of flow = 0.134(Ft.)
Average velocity = 2.148(Ft/s)
Total irregular channel flow = 0.814(CFS)
Irregular channel normal depth above invert elev. = 0.134(Ft.)
Average velocity of channel(s) = 2.148(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Rainfall intensity = 4.097(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for total area

(Q=KCIA) is C = 0.820 CA = 0.355
Subarea runoff = 1.358(CFS) for 0.409(Ac.)
Total runoff = 1.455(CFS) Total area = 0.433(Ac.)
Depth of flow = 0.167(Ft.), Average velocity = 2.483(Ft/s)

Process from Point/Station 17.000 to Point/Station 17.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 2
Stream flow area = 0.433(Ac.)
Runoff from this stream = 1.455(CFS)
Time of concentration = 4.98 min.
Rainfall intensity = 4.097(In/Hr)
Summary of stream data:

| Stream No. | Flow rate (CFS) | TC (min) | Rainfall Intensity (In/Hr) |
|------------|-----------------|----------|----------------------------|
| 1 | 0.815 | 6.99 | 3.290 |
| 2 | 1.455 | 4.98 | 4.097 |

Qmax(1) =
1.000 * 1.000 * 0.815) +
0.803 * 1.000 * 1.455) + = 1.983

Qmax(2) =
1.000 * 0.712 * 0.815) +
1.000 * 1.000 * 1.455) + = 2.034

Total of 2 streams to confluence:
Flow rates before confluence point:
0.815 1.455
Maximum flow rates at confluence using above data:
1.983 2.034
Area of streams before confluence:
0.302 0.433
Results of confluence:
Total flow rate = 2.034(CFS)
Time of concentration = 4.975 min.
Effective stream area after confluence = 0.735(Ac.)

Process from Point/Station 17.000 to Point/Station 11.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 656.400(Ft.)
Downstream point/station elevation = 655.400(Ft.)
Pipe length = 196.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 2.034(CFS)
Nearest computed pipe diameter = 12.00(In.)
Calculated individual pipe flow = 2.034(CFS)
Normal flow depth in pipe = 8.11(In.)
Flow top width inside pipe = 11.23(In.)
Critical Depth = 7.30(In.)
Pipe flow velocity = 3.60(Ft/s)
Travel time through pipe = 0.91 min.
Time of concentration (TC) = 5.88 min.

Process from Point/Station 11.000 to Point/Station 11.000
**** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area = 0.735(Ac.)
Runoff from this stream = 2.034(CFS)
Time of concentration = 5.88 min.
Rainfall intensity = 3.677(In/Hr)

Summary of stream data:

| Stream No. | Flow rate (CFS) | TC (min) | Rainfall Intensity (In/Hr) |
|------------|-----------------|----------|----------------------------|
| 1 | 5.387 | 8.51 | 2.898 |
| 2 | 2.034 | 5.88 | 3.677 |
| Qmax(1) = | | | |
| | 1.000 * | 1.000 * | 5.387) + |
| | 0.788 * | 1.000 * | 2.034) + = 6.991 |
| Qmax(2) = | | | |
| | 1.000 * | 0.691 * | 5.387) + |
| | 1.000 * | 1.000 * | 2.034) + = 5.759 |

Total of 2 main streams to confluence:

Flow rates before confluence point:

5.387 2.034

Maximum flow rates at confluence using above data:

6.991 5.759

Area of streams before confluence:

1.818 0.735

Results of confluence:

Total flow rate = 6.991(CFS)

Time of concentration = 8.508 min.

Effective stream area after confluence = 2.553(Ac.)

 Process from Point/Station 11.000 to Point/Station 20.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 655.400(Ft.)
 Downstream point/station elevation = 654.200(Ft.)
 Pipe length = 246.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 6.991(CFS)
 Nearest computed pipe diameter = 18.00(In.)
 Calculated individual pipe flow = 6.991(CFS)
 Normal flow depth in pipe = 14.04(In.)
 Flow top width inside pipe = 14.91(In.)
 Critical Depth = 12.28(In.)
 Pipe flow velocity = 4.73(Ft/s)
 Travel time through pipe = 0.87 min.
 Time of concentration (TC) = 9.38 min.

 Process from Point/Station 20.000 to Point/Station 20.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 2.553(Ac.)
 Runoff from this stream = 6.991(CFS)
 Time of concentration = 9.38 min.
 Rainfall intensity = 2.722(In/Hr)

 Process from Point/Station 21.000 to Point/Station 22.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000

[COMMERCIAL area type]
 (General Commercial)
 Impervious value, Ai = 0.850
 Sub-Area C Value = 0.820

Initial subarea total flow distance = 58.000(Ft.)
 Highest elevation = 663.400(Ft.)
 Lowest elevation = 662.600(Ft.)
 Elevation difference = 0.800(Ft.) Slope = 1.379 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 60.00 (Ft)
 for the top area slope value of 1.38 %, in a development type of
 General Commercial
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 3.51 minutes
 $TC = [1.8*(1.1-C)*distance(Ft.)^{.5}]/(%\ slope^{(1/3)})]$
 $TC = [1.8*(1.1-0.8200)*(60.000^{.5})]/(1.379^{(1/3)}) = 3.51$
 Rainfall intensity (I) = 5.133(In/Hr) for a 2.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.820
 Subarea runoff = 0.185(CFS)
 Total initial stream area = 0.044(Ac.)

 Process from Point/Station 22.000 to Point/Station 20.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

 Estimated mean flow rate at midpoint of channel = 1.085(CFS)
 Depth of flow = 0.085(Ft.), Average velocity = 2.721(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :

| Point number | 'X' coordinate | 'Y' coordinate |
|--------------|----------------|----------------|
| 1 | 0.00 | 0.27 |
| 2 | 18.60 | 0.00 |
| 3 | 53.60 | 0.87 |

 Manning's 'N' friction factor = 0.013

Sub-Channel flow = 1.085(CFS)
 ' ' flow top width = 9.328(Ft.)
 ' ' velocity = 2.721(Ft/s)
 ' ' area = 0.399(Sq.Ft)
 ' ' Froude number = 2.320

Upstream point elevation = 662.600(Ft.)
 Downstream point elevation = 660.400(Ft.)
 Flow length = 58.000(Ft.)
 Travel time = 0.36 min.
 Time of concentration = 3.86 min.
 Depth of flow = 0.085(Ft.)
 Average velocity = 2.721(Ft/s)
 Total irregular channel flow = 1.085(CFS)
 Irregular channel normal depth above invert elev. = 0.085(Ft.)
 Average velocity of channel(s) = 2.721(Ft/s)
 Adding area flow to channel
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [COMMERCIAL area type]
 (General Commercial)
 Impervious value, Ai = 0.850
 Sub-Area C Value = 0.820
 Rainfall intensity = 4.824(In/Hr) for a 2.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.820 CA = 0.399
 Subarea runoff = 1.737(CFS) for 0.442(Ac.)
 Total runoff = 1.922(CFS) Total area = 0.486(Ac.)
 Depth of flow = 0.106(Ft.), Average velocity = 3.139(Ft/s)

 Process from Point/Station 20.000 to Point/Station 20.000
 **** CONFLUENCE OF MINOR STREAMS ****

 Along Main Stream number: 1 in normal stream number 2

Stream flow area = 0.486(Ac.)
 Runoff from this stream = 1.922(CFS)
 Time of concentration = 3.86 min.
 Rainfall intensity = 4.824(In/Hr)
 Summary of stream data:

| Stream No. | Flow rate (CFS) | TC (min) | Rainfall Intensity (In/Hr) |
|------------|-----------------|----------|----------------------------|
| 1 | 6.991 | 9.38 | 2.722 |
| 2 | 1.922 | 3.86 | 4.824 |
| Qmax(1) = | | | |
| | 1.000 * | 1.000 * | 6.991) + |
| | 0.564 * | 1.000 * | 1.922) + = 8.076 |
| Qmax(2) = | | | |
| | 1.000 * | 0.412 * | 6.991) + |
| | 1.000 * | 1.000 * | 1.922) + = 4.802 |

Total of 2 streams to confluence:
 Flow rates before confluence point:
 6.991 1.922
 Maximum flow rates at confluence using above data:
 8.076 4.802
 Area of streams before confluence:
 2.553 0.486
 Results of confluence:
 Total flow rate = 8.076(CFS)
 Time of concentration = 9.376 min.
 Effective stream area after confluence = 3.039(Ac.)

 Process from Point/Station 20.000 to Point/Station 23.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 654.200(Ft.)
 Downstream point/station elevation = 653.260(Ft.)
 Pipe length = 86.00(Ft.) Manning's N = 0.013
 No. of pipes = 3 Required pipe flow = 8.076(CFS)
 Nearest computed pipe diameter = 12.00(In.)
 Calculated individual pipe flow = 2.692(CFS)
 Normal flow depth in pipe = 7.56(In.)
 Flow top width inside pipe = 11.59(In.)
 Critical Depth = 8.44(In.)
 Pipe flow velocity = 5.17(Ft/s)
 Travel time through pipe = 0.28 min.
 Time of concentration (TC) = 9.65 min.
 End of computations, total study area = 3.039 (Ac.)

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 04/02/13

Outfall A
Basin A, B, C, and D
50 Year Rainfall Event

***** Hydrology Study Control Information *****

Program License Serial Number 4012

Rational hydrology study storm event year is 50.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 2.750
24 hour precipitation(inches) = 5.750
P6/P24 = 47.8%
San Diego hydrology manual 'C' values used

Process from Point/Station 1.000 to Point/Station 2.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Initial subarea total flow distance = 56.000(Ft.)
Highest elevation = 662.000(Ft.)
Lowest elevation = 661.500(Ft.)
Elevation difference = 0.500(Ft.) Slope = 0.893 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 60.00 (Ft)
for the top area slope value of 0.89 %, in a development type of
General Commercial
In Accordance With Figure 3-3
Initial Area Time of Concentration = 4.05 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.8200)*(60.000^0.5)]/(0.893^(1/3))= 4.05
Rainfall intensity (I) = 8.295(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.820
Subarea runoff = 0.170(CFS)
Total initial stream area = 0.025(Ac.)

Process from Point/Station 2.000 to Point/Station 3.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.398(CFS)
Depth of flow = 0.086(Ft.), Average velocity = 1.060(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :

| Point number | 'X' coordinate | 'Y' coordinate |
|--------------|----------------|----------------|
| 1 | 0.00 | 0.45 |
| 2 | 45.00 | 0.00 |
| 3 | 45.50 | 0.50 |

Manning's 'N' friction factor = 0.013

```
-----
Sub-Channel flow = 0.398(CFS)
'   '   flow top width = 8.710(Ft.)
'   '   velocity= 1.060(Ft/s)
'   '   area = 0.376(Sq.Ft)
'   '   Froude number = 0.899
```

Upstream point elevation = 661.500(Ft.)
 Downstream point elevation = 661.300(Ft.)
 Flow length = 35.000(Ft.)
 Travel time = 0.55 min.
 Time of concentration = 4.60 min.
 Depth of flow = 0.086(Ft.)
 Average velocity = 1.060(Ft/s)
 Total irregular channel flow = 0.398(CFS)
 Irregular channel normal depth above invert elev. = 0.086(Ft.)
 Average velocity of channel(s) = 1.060(Ft/s)

Adding area flow to channel
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [COMMERCIAL area type]
 (General Commercial)
 Impervious value, Ai = 0.850
 Sub-Area C Value = 0.820
 Rainfall intensity = 7.641(In/Hr) for a 50.0 year storm
 Effective runoff coefficient used for total area
 (Q=K CIA) is C = 0.820 CA = 0.075
 Subarea runoff = 0.406(CFS) for 0.067(Ac.)
 Total runoff = 0.576(CFS) Total area = 0.092(Ac.)
 Depth of flow = 0.099(Ft.), Average velocity = 1.162(Ft/s)

```
*****
Process from Point/Station 3.000 to Point/Station 4.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
```

```
-----
Upstream point/station elevation = 661.300(Ft.)
Downstream point/station elevation = 660.100(Ft.)
Pipe length = 30.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.576(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.576(CFS)
Normal flow depth in pipe = 3.05(In.)
Flow top width inside pipe = 6.00(In.)
Critical Depth = 4.64(In.)
Pipe flow velocity = 5.75(Ft/s)
Travel time through pipe = 0.09 min.
Time of concentration (TC) = 4.69 min.
```

```
*****
Process from Point/Station 4.000 to Point/Station 4.000
**** SUBAREA FLOW ADDITION ****
```

```
-----
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type ]
(General Commercial )
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Time of concentration = 4.69 min.
Rainfall intensity = 7.549(In/Hr) for a 50.0 year storm
```

Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.820 CA = 0.823
Subarea runoff = 5.639(CFS) for 0.912(Ac.)
Total runoff = 6.215(CFS) Total area = 1.004(Ac.)

Process from Point/Station 4.000 to Point/Station 5.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 6.249(CFS)
Depth of flow = 0.448(Ft.), Average velocity = 1.860(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 0.53
2 2.10 0.00
3 7.80 0.00
4 9.90 0.53
Manning's 'N' friction factor = 0.030

Sub-Channel flow = 6.249(CFS)
' ' flow top width = 9.287(Ft.)
' ' velocity = 1.860(Ft/s)
' ' area = 3.360(Sq.Ft)
' ' Froude number = 0.545

Upstream point elevation = 660.100(Ft.)
Downstream point elevation = 658.900(Ft.)
Flow length = 216.000(Ft.)
Travel time = 1.94 min.
Time of concentration = 6.63 min.
Depth of flow = 0.448(Ft.)
Average velocity = 1.860(Ft/s)
Total irregular channel flow = 6.249(CFS)
Irregular channel normal depth above invert elev. = 0.448(Ft.)
Average velocity of channel(s) = 1.860(Ft/s)

Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820

The area added to the existing stream causes a
a lower flow rate of Q = 5.405(CFS)
therefore the upstream flow rate of Q = 6.215(CFS) is being used
Rainfall intensity = 6.042(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.820 CA = 0.895
Subarea runoff = 0.000(CFS) for 0.087(Ac.)
Total runoff = 6.215(CFS) Total area = 1.091(Ac.)
Depth of flow = 0.447(Ft.), Average velocity = 1.857(Ft/s)

Process from Point/Station 5.000 to Point/Station 6.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 657.200(Ft.)
Downstream point/station elevation = 655.700(Ft.)
Pipe length = 293.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 6.215(CFS)
Nearest computed pipe diameter = 18.00(In.)
Calculated individual pipe flow = 6.215(CFS)
Normal flow depth in pipe = 12.48(In.)
Flow top width inside pipe = 16.60(In.)
Critical Depth = 11.56(In.)

Pipe flow velocity = 4.75(Ft/s)
Travel time through pipe = 1.03 min.
Time of concentration (TC) = 7.65 min.

Process from Point/Station 6.000 to Point/Station 6.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 1.091(Ac.)
Runoff from this stream = 6.215(CFS)
Time of concentration = 7.65 min.
Rainfall intensity = 5.505(In/Hr)

Process from Point/Station 7.000 to Point/Station 8.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Initial subarea total flow distance = 50.000(Ft.)
Highest elevation = 663.400(Ft.)
Lowest elevation = 662.800(Ft.)
Elevation difference = 0.600(Ft.) Slope = 1.200 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 60.00 (Ft)
for the top area slope value of 1.20 %, in a development type of
General Commercial
In Accordance With Figure 3-3
Initial Area Time of Concentration = 3.67 minutes
TC = $[1.8 * (1.1 - C) * \text{distance}(\text{Ft.})^{.5}] / (\% \text{ slope}^{(1/3)})$
TC = $[1.8 * (1.1 - 0.8200) * (60.000^{.5})] / (1.200^{(1/3)}) = 3.67$
Rainfall intensity (I) = 8.839(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.820
Subarea runoff = 0.203(CFS)
Total initial stream area = 0.028(Ac.)

Process from Point/Station 8.000 to Point/Station 6.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.954(CFS)
Depth of flow = 0.095(Ft.), Average velocity = 1.229(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 0.35
2 30.00 0.00
3 60.00 0.35
Manning's 'N' friction factor = 0.013

Sub-Channel flow = 0.954(CFS)
' ' flow top width = 16.310(Ft.)
' ' velocity = 1.229(Ft/s)
' ' area = 0.776(Sq.Ft)
' ' Froude number = 0.993

Upstream point elevation = 662.800(Ft.)
Downstream point elevation = 660.700(Ft.)
Flow length = 313.000(Ft.)
Travel time = 4.24 min.

Time of concentration = 7.92 min.
 Depth of flow = 0.095(Ft.)
 Average velocity = 1.229(Ft/s)
 Total irregular channel flow = 0.954(CFS)
 Irregular channel normal depth above invert elev. = 0.095(Ft.)
 Average velocity of channel(s) = 1.229(Ft/s)
 Adding area flow to channel
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [COMMERCIAL area type]
 (General Commercial)
 Impervious value, Ai = 0.850
 Sub-Area C Value = 0.820
 Rainfall intensity = 5.386(In/Hr) for a 50.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.820 CA = 0.302
 Subarea runoff = 1.422(CFS) for 0.340(Ac.)
 Total runoff = 1.625(CFS) Total area = 0.368(Ac.)
 Depth of flow = 0.116(Ft.), Average velocity = 1.404(Ft/s)

 Process from Point/Station 6.000 to Point/Station 6.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 0.368(Ac.)
 Runoff from this stream = 1.625(CFS)
 Time of concentration = 7.92 min.
 Rainfall intensity = 5.386(In/Hr)

 Process from Point/Station 9.000 to Point/Station 10.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [COMMERCIAL area type]
 (General Commercial)
 Impervious value, Ai = 0.850
 Sub-Area C Value = 0.820
 Initial subarea total flow distance = 60.000(Ft.)
 Highest elevation = 663.300(Ft.)
 Lowest elevation = 661.600(Ft.)
 Elevation difference = 1.700(Ft.) Slope = 2.833 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 85.00 (Ft)
 for the top area slope value of 2.83 %, in a development type of
 General Commercial
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 3.28 minutes
 $TC = [1.8 * (1.1 - C) * distance(Ft.)^{.5}] / (\% slope^{(1/3)})$
 $TC = [1.8 * (1.1 - 0.8200) * (85.000^{.5})] / (2.833^{(1/3)}) = 3.28$
 Rainfall intensity (I) = 9.502(In/Hr) for a 50.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.820
 Subarea runoff = 0.296(CFS)
 Total initial stream area = 0.038(Ac.)

 Process from Point/Station 10.000 to Point/Station 10.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000

Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Time of concentration = 3.28 min.
Rainfall intensity = 9.502(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.820 CA = 0.250
Subarea runoff = 2.080(CFS) for 0.267(Ac.)
Total runoff = 2.377(CFS) Total area = 0.305(Ac.)

Process from Point/Station 10.000 to Point/Station 6.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 2.403(CFS)
Depth of flow = 0.217(Ft.), Average velocity = 1.261(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 0.50
2 0.50 0.00
3 8.83 0.00
4 10.33 0.50
Manning's 'N' friction factor = 0.030

Sub-Channel flow = 2.403(CFS)
' ' flow top width = 9.199(Ft.)
' ' velocity = 1.261(Ft/s)
' ' area = 1.905(Sq.Ft)
' ' Froude number = 0.488

Upstream point elevation = 661.600(Ft.)
Downstream point elevation = 660.700(Ft.)
Flow length = 167.000(Ft.)
Travel time = 2.21 min.
Time of concentration = 5.49 min.
Depth of flow = 0.217(Ft.)
Average velocity = 1.261(Ft/s)
Total irregular channel flow = 2.403(CFS)
Irregular channel normal depth above invert elev. = 0.217(Ft.)
Average velocity of channel(s) = 1.261(Ft/s)
Adding area flow to channel

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
The area added to the existing stream causes a
a lower flow rate of Q = 2.008(CFS)
therefore the upstream flow rate of Q = 2.377(CFS) is being used
Rainfall intensity = 6.821(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.820 CA = 0.294
Subarea runoff = 0.000(CFS) for 0.054(Ac.)
Total runoff = 2.377(CFS) Total area = 0.359(Ac.)
Depth of flow = 0.216(Ft.), Average velocity = 1.256(Ft/s)

Process from Point/Station 6.000 to Point/Station 6.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
Stream flow area = 0.359(Ac.)

Runoff from this stream = 2.377(CFS)
 Time of concentration = 5.49 min.
 Rainfall intensity = 6.821(In/Hr)
 Summary of stream data:

| Stream No. | Flow rate (CFS) | TC (min) | Rainfall Intensity (In/Hr) |
|------------|-----------------|----------|----------------------------|
| 1 | 6.215 | 7.65 | 5.505 |
| 2 | 1.625 | 7.92 | 5.386 |
| 3 | 2.377 | 5.49 | 6.821 |

Qmax(1) =
 1.000 * 1.000 * 6.215) +
 1.000 * 0.967 * 1.625) +
 0.807 * 1.000 * 2.377) + = 9.705

Qmax(2) =
 0.978 * 1.000 * 6.215) +
 1.000 * 1.000 * 1.625) +
 0.790 * 1.000 * 2.377) + = 9.583

Qmax(3) =
 1.000 * 0.717 * 6.215) +
 1.000 * 0.693 * 1.625) +
 1.000 * 1.000 * 2.377) + = 7.962

Total of 3 streams to confluence:
 Flow rates before confluence point:
 6.215 1.625 2.377
 Maximum flow rates at confluence using above data:
 9.705 9.583 7.962
 Area of streams before confluence:
 1.091 0.368 0.359

Results of confluence:
 Total flow rate = 9.705(CFS)
 Time of concentration = 7.655 min.
 Effective stream area after confluence = 1.818(Ac.)

 Process from Point/Station 6.000 to Point/Station 11.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 655.700(Ft.)
 Downstream point/station elevation = 655.400(Ft.)
 Pipe length = 57.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 9.705(CFS)
 Nearest computed pipe diameter = 21.00(In.)
 Calculated individual pipe flow = 9.705(CFS)
 Normal flow depth in pipe = 14.79(In.)
 Flow top width inside pipe = 19.17(In.)
 Critical Depth = 13.91(In.)
 Pipe flow velocity = 5.36(Ft/s)
 Travel time through pipe = 0.18 min.
 Time of concentration (TC) = 7.83 min.

 Process from Point/Station 11.000 to Point/Station 11.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
 In Main Stream number: 1
 Stream flow area = 1.818(Ac.)
 Runoff from this stream = 9.705(CFS)
 Time of concentration = 7.83 min.
 Rainfall intensity = 5.424(In/Hr)
 Program is now starting with Main Stream No. 2

 Process from Point/Station 12.000 to Point/Station 13.000

**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Initial subarea total flow distance = 59.000(Ft.)
Highest elevation = 662.000(Ft.)
Lowest elevation = 661.500(Ft.)
Elevation difference = 0.500(Ft.) Slope = 0.847 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 60.00 (Ft)
for the top area slope value of 0.85 %, in a development type of
General Commercial
In Accordance With Figure 3-3
Initial Area Time of Concentration = 4.13 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.8200)*(60.000^0.5)]/(0.847^(1/3))= 4.13
Rainfall intensity (I) = 8.201(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.820
Subarea runoff = 0.208(CFS)
Total initial stream area = 0.031(Ac.)

Process from Point/Station 13.000 to Point/Station 14.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.387(CFS)
Depth of flow = 0.096(Ft.), Average velocity = 1.138(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 0.64
2 46.50 0.00
3 47.00 0.50
Manning's 'N' friction factor = 0.013

Sub-Channel flow = 0.387(CFS)
' ' flow top width = 7.077(Ft.)
' ' velocity= 1.138(Ft/s)
' ' area = 0.340(Sq.Ft)
' ' Froude number = 0.915

Upstream point elevation = 661.500(Ft.)
Downstream point elevation = 661.300(Ft.)
Flow length = 35.000(Ft.)
Travel time = 0.51 min.
Time of concentration = 4.64 min.
Depth of flow = 0.096(Ft.)
Average velocity = 1.138(Ft/s)
Total irregular channel flow = 0.387(CFS)
Irregular channel normal depth above invert elev. = 0.096(Ft.)
Average velocity of channel(s) = 1.138(Ft/s)

Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Rainfall intensity = 7.604(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.820 CA = 0.069

Subarea runoff = 0.315(CFS) for 0.053(Ac.)
Total runoff = 0.524(CFS) Total area = 0.084(Ac.)
Depth of flow = 0.108(Ft.), Average velocity = 1.227(Ft/s)

Process from Point/Station 14.000 to Point/Station 15.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 661.300(Ft.)
Downstream point/station elevation = 660.900(Ft.)
Pipe length = 42.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 0.524(CFS)
Nearest computed pipe diameter = 6.00(In.)
Calculated individual pipe flow = 0.524(CFS)
Normal flow depth in pipe = 4.70(In.)
Flow top width inside pipe = 4.94(In.)
Critical Depth = 4.43(In.)
Pipe flow velocity = 3.18(Ft/s)
Travel time through pipe = 0.22 min.
Time of concentration (TC) = 4.86 min.

Process from Point/Station 15.000 to Point/Station 15.000
**** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Time of concentration = 4.86 min.
Rainfall intensity = 7.380(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.820 CA = 0.143
Subarea runoff = 0.535(CFS) for 0.091(Ac.)
Total runoff = 1.059(CFS) Total area = 0.175(Ac.)

Process from Point/Station 15.000 to Point/Station 16.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 1.277(CFS)
Depth of flow = 0.200(Ft.), Average velocity = 0.727(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 0.50
2 2.00 0.00
3 10.00 0.00
4 12.00 0.50
Manning's 'N' friction factor = 0.030

Sub-Channel flow = 1.277(CFS)
' ' flow top width = 9.598(Ft.)
' ' velocity = 0.727(Ft/s)
' ' area = 1.757(Sq.Ft)
' ' Froude number = 0.299

Upstream point elevation = 660.900(Ft.)
Downstream point elevation = 660.800(Ft.)
Flow length = 48.000(Ft.)
Travel time = 1.10 min.
Time of concentration = 5.96 min.
Depth of flow = 0.200(Ft.)

Average velocity = 0.727(Ft/s)
 Total irregular channel flow = 1.277(CFS)
 Irregular channel normal depth above invert elev. = 0.200(Ft.)
 Average velocity of channel(s) = 0.727(Ft/s)
 Adding area flow to channel
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [COMMERCIAL area type]
 (General Commercial)
 Impervious value, Ai = 0.850
 Sub-Area C Value = 0.820
 Rainfall intensity = 6.469(In/Hr) for a 50.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.820 CA = 0.216
 Subarea runoff = 0.336(CFS) for 0.088(Ac.)
 Total runoff = 1.395(CFS) Total area = 0.263(Ac.)
 Depth of flow = 0.210(Ft.), Average velocity = 0.750(Ft/s)

 Process from Point/Station 16.000 to Point/Station 17.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 656.900(Ft.)
 Downstream point/station elevation = 656.400(Ft.)
 Pipe length = 108.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 1.395(CFS)
 Nearest computed pipe diameter = 12.00(In.)
 Calculated individual pipe flow = 1.395(CFS)
 Normal flow depth in pipe = 6.53(In.)
 Flow top width inside pipe = 11.95(In.)
 Critical Depth = 5.99(In.)
 Pipe flow velocity = 3.19(Ft/s)
 Travel time through pipe = 0.56 min.
 Time of concentration (TC) = 6.52 min.

 Process from Point/Station 17.000 to Point/Station 17.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [COMMERCIAL area type]
 (General Commercial)
 Impervious value, Ai = 0.850
 Sub-Area C Value = 0.820
 Time of concentration = 6.52 min.
 Rainfall intensity = 6.103(In/Hr) for a 50.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.820 CA = 0.248
 Subarea runoff = 0.116(CFS) for 0.039(Ac.)
 Total runoff = 1.511(CFS) Total area = 0.302(Ac.)

 Process from Point/Station 17.000 to Point/Station 17.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 1
 Stream flow area = 0.302(Ac.)
 Runoff from this stream = 1.511(CFS)
 Time of concentration = 6.52 min.
 Rainfall intensity = 6.103(In/Hr)

Process from Point/Station 18.000 to Point/Station 19.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Initial subarea total flow distance = 35.000(Ft.)
Highest elevation = 663.000(Ft.)
Lowest elevation = 662.600(Ft.)
Elevation difference = 0.400(Ft.) Slope = 1.143 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 60.00 (Ft)
for the top area slope value of 1.14 %, in a development type of
General Commercial
In Accordance With Figure 3-3
Initial Area Time of Concentration = 3.73 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.8200)*(60.000^0.5)/(1.143^(1/3))]= 3.73
Rainfall intensity (I) = 8.747(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.820
Subarea runoff = 0.172(CFS)
Total initial stream area = 0.024(Ac.)

Process from Point/Station 19.000 to Point/Station 17.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 1.436(CFS)
Depth of flow = 0.166(Ft.), Average velocity = 2.475(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate
1 0.00 1.46
2 60.00 0.00
3 60.50 0.50
Manning's 'N' friction factor = 0.013

Sub-Channel flow = 1.436(CFS)
' ' flow top width = 6.989(Ft.)
' ' velocity = 2.475(Ft/s)
' ' area = 0.580(Sq.Ft)
' ' Froude number = 1.514

Upstream point elevation = 662.600(Ft.)
Downstream point elevation = 660.500(Ft.)
Flow length = 160.000(Ft.)
Travel time = 1.08 min.
Time of concentration = 4.81 min.
Depth of flow = 0.166(Ft.)
Average velocity = 2.475(Ft/s)
Total irregular channel flow = 1.436(CFS)
Irregular channel normal depth above invert elev. = 0.166(Ft.)
Average velocity of channel(s) = 2.475(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Rainfall intensity = 7.428(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for total area

(Q=KCIA) is C = 0.820 CA = 0.355
 Subarea runoff = 2.465(CFS) for 0.409(Ac.)
 Total runoff = 2.637(CFS) Total area = 0.433(Ac.)
 Depth of flow = 0.209(Ft.), Average velocity = 2.882(Ft/s)

 Process from Point/Station 17.000 to Point/Station 17.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 2 in normal stream number 2
 Stream flow area = 0.433(Ac.)
 Runoff from this stream = 2.637(CFS)
 Time of concentration = 4.81 min.
 Rainfall intensity = 7.428(In/Hr)
 Summary of stream data:

| Stream No. | Flow rate (CFS) | TC (min) | Rainfall Intensity (In/Hr) |
|------------|-----------------|----------|----------------------------|
| 1 | 1.511 | 6.52 | 6.103 |
| 2 | 2.637 | 4.81 | 7.428 |
| Qmax(1) = | | | |
| | 1.000 * | 1.000 * | 1.511) + |
| | 0.822 * | 1.000 * | 2.637) + = 3.678 |
| Qmax(2) = | | | |
| | 1.000 * | 0.737 * | 1.511) + |
| | 1.000 * | 1.000 * | 2.637) + = 3.752 |

Total of 2 streams to confluence:
 Flow rates before confluence point:
 1.511 2.637
 Maximum flow rates at confluence using above data:
 3.678 3.752
 Area of streams before confluence:
 0.302 0.433
 Results of confluence:
 Total flow rate = 3.752(CFS)
 Time of concentration = 4.811 min.
 Effective stream area after confluence = 0.735(Ac.)

 Process from Point/Station 17.000 to Point/Station 11.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 656.400(Ft.)
 Downstream point/station elevation = 655.400(Ft.)
 Pipe length = 196.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 3.752(CFS)
 Nearest computed pipe diameter = 15.00(In.)
 Calculated individual pipe flow = 3.752(CFS)
 Normal flow depth in pipe = 10.27(In.)
 Flow top width inside pipe = 13.94(In.)
 Critical Depth = 9.39(In.)
 Pipe flow velocity = 4.19(Ft/s)
 Travel time through pipe = 0.78 min.
 Time of concentration (TC) = 5.59 min.

 Process from Point/Station 11.000 to Point/Station 11.000
 **** CONFLUENCE OF MAIN STREAMS ****

The following data inside Main Stream is listed:
 In Main Stream number: 2
 Stream flow area = 0.735(Ac.)
 Runoff from this stream = 3.752(CFS)
 Time of concentration = 5.59 min.
 Rainfall intensity = 6.742(In/Hr)

Summary of stream data:

| Stream No. | Flow rate (CFS) | TC (min) | Rainfall Intensity (In/Hr) |
|------------|-----------------|----------|----------------------------|
|------------|-----------------|----------|----------------------------|

| | | | |
|---|-------|------|-------|
| 1 | 9.705 | 7.83 | 5.424 |
| 2 | 3.752 | 5.59 | 6.742 |

Qmax(1) =

| | | | |
|---------|---------|------------|--------|
| 1.000 * | 1.000 * | 9.705) + | |
| 0.805 * | 1.000 * | 3.752) + = | 12.723 |

Qmax(2) =

| | | | |
|---------|---------|------------|--------|
| 1.000 * | 0.714 * | 9.705) + | |
| 1.000 * | 1.000 * | 3.752) + = | 10.680 |

Total of 2 main streams to confluence:

Flow rates before confluence point:

9.705 3.752

Maximum flow rates at confluence using above data:

12.723 10.680

Area of streams before confluence:

1.818 0.735

Results of confluence:

Total flow rate = 12.723(CFS)

Time of concentration = 7.832 min.

Effective stream area after confluence = 2.553(Ac.)

 Process from Point/Station 11.000 to Point/Station 20.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 655.400(Ft.)
 Downstream point/station elevation = 654.200(Ft.)
 Pipe length = 246.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 12.723(CFS)
 Nearest computed pipe diameter = 24.00(In.)
 Calculated individual pipe flow = 12.723(CFS)
 Normal flow depth in pipe = 16.31(In.)
 Flow top width inside pipe = 22.40(In.)
 Critical Depth = 15.39(In.)
 Pipe flow velocity = 5.59(Ft/s)
 Travel time through pipe = 0.73 min.
 Time of concentration (TC) = 8.56 min.

 Process from Point/Station 20.000 to Point/Station 20.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1

Stream flow area = 2.553(Ac.)
 Runoff from this stream = 12.723(CFS)
 Time of concentration = 8.56 min.
 Rainfall intensity = 5.120(In/Hr)

 Process from Point/Station 21.000 to Point/Station 22.000
 **** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000

[COMMERCIAL area type]
 (General Commercial)

Impervious value, Ai = 0.850

Sub-Area C Value = 0.820

Initial subarea total flow distance = 58.000(Ft.)
 Highest elevation = 663.400(Ft.)
 Lowest elevation = 662.600(Ft.)
 Elevation difference = 0.800(Ft.) Slope = 1.379 %
 INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
 The maximum overland flow distance is 60.00 (Ft)
 for the top area slope value of 1.38 %, in a development type of
 General Commercial
 In Accordance With Figure 3-3
 Initial Area Time of Concentration = 3.51 minutes
 $TC = [1.8*(1.1-C)*distance(Ft.)^{.5}]/(%\ slope^{(1/3)})]$
 $TC = [1.8*(1.1-0.8200)*(60.000^{.5})/(1.379^{(1/3)})] = 3.51$
 Rainfall intensity (I) = 9.107(In/Hr) for a 50.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.820
 Subarea runoff = 0.329(CFS)
 Total initial stream area = 0.044(Ac.)

 Process from Point/Station 22.000 to Point/Station 20.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

 Estimated mean flow rate at midpoint of channel = 1.931(CFS)
 Depth of flow = 0.106(Ft.), Average velocity = 3.143(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :

| Point number | 'X' coordinate | 'Y' coordinate |
|--------------|----------------|----------------|
| 1 | 0.00 | 0.27 |
| 2 | 18.60 | 0.00 |
| 3 | 53.60 | 0.87 |

 Manning's 'N' friction factor = 0.013

Sub-Channel flow = 1.931(CFS)
 ' ' flow top width = 11.580(Ft.)
 ' ' velocity = 3.143(Ft/s)
 ' ' area = 0.614(Sq.Ft)
 ' ' Froude number = 2.405

Upstream point elevation = 662.600(Ft.)
 Downstream point elevation = 660.400(Ft.)
 Flow length = 58.000(Ft.)
 Travel time = 0.31 min.
 Time of concentration = 3.81 min.
 Depth of flow = 0.106(Ft.)
 Average velocity = 3.143(Ft/s)
 Total irregular channel flow = 1.931(CFS)
 Irregular channel normal depth above invert elev. = 0.106(Ft.)
 Average velocity of channel(s) = 3.143(Ft/s)
 Adding area flow to channel
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [COMMERCIAL area type]
 (General Commercial)
 Impervious value, Ai = 0.850
 Sub-Area C Value = 0.820
 Rainfall intensity = 8.627(In/Hr) for a 50.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.820 CA = 0.399
 Subarea runoff = 3.109(CFS) for 0.442(Ac.)
 Total runoff = 3.438(CFS) Total area = 0.486(Ac.)
 Depth of flow = 0.132(Ft.), Average velocity = 3.631(Ft/s)

 Process from Point/Station 20.000 to Point/Station 20.000
 **** CONFLUENCE OF MINOR STREAMS ****

 Along Main Stream number: 1 in normal stream number 2

Stream flow area = 0.486(Ac.)
 Runoff from this stream = 3.438(CFS)
 Time of concentration = 3.81 min.
 Rainfall intensity = 8.627(In/Hr)
 Summary of stream data:

| Stream No. | Flow rate (CFS) | TC (min) | Rainfall Intensity (In/Hr) |
|------------|-----------------|----------|----------------------------|
| 1 | 12.723 | 8.56 | 5.120 |
| 2 | 3.438 | 3.81 | 8.627 |
| Qmax(1) = | | | |
| | 1.000 * | 1.000 * | 12.723) + |
| | 0.594 * | 1.000 * | 3.438) + = 14.764 |
| Qmax(2) = | | | |
| | 1.000 * | 0.445 * | 12.723) + |
| | 1.000 * | 1.000 * | 3.438) + = 9.105 |

Total of 2 streams to confluence:
 Flow rates before confluence point:
 12.723 3.438
 Maximum flow rates at confluence using above data:
 14.764 9.105
 Area of streams before confluence:
 2.553 0.486
 Results of confluence:
 Total flow rate = 14.764(CFS)
 Time of concentration = 8.565 min.
 Effective stream area after confluence = 3.039(Ac.)

 Process from Point/Station 20.000 to Point/Station 23.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 654.200(Ft.)
 Downstream point/station elevation = 653.260(Ft.)
 Pipe length = 86.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 14.764(CFS)
 Nearest computed pipe diameter = 21.00(In.)
 Calculated individual pipe flow = 14.764(CFS)
 Normal flow depth in pipe = 15.45(In.)
 Flow top width inside pipe = 18.52(In.)
 Critical Depth = 17.10(In.)
 Pipe flow velocity = 7.78(Ft/s)
 Travel time through pipe = 0.18 min.
 Time of concentration (TC) = 8.75 min.
 End of computations, total study area = 3.039 (Ac.)

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 04/02/13

Outfall B
Basin C1
2 Year Rainfall Event

***** Hydrology Study Control Information *****

Program License Serial Number 4012

Rational hydrology study storm event year is 2.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 1.550
24 hour precipitation(inches) = 2.400
P6/P24 = 64.6%
San Diego hydrology manual 'C' values used

Process from Point/Station 24.000 to Point/Station 25.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Initial subarea total flow distance = 75.000(Ft.)
Highest elevation = 663.600(Ft.)
Lowest elevation = 662.300(Ft.)
Elevation difference = 1.300(Ft.) Slope = 1.733 %
Top of Initial Area Slope adjusted by User to 2.034 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 75.00 (Ft)
for the top area slope value of 2.03 %, in a development type of
General Commercial
In Accordance With Figure 3-3
Initial Area Time of Concentration = 3.44 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.8200)*(75.000^0.5)]/(2.034^(1/3))= 3.44
Rainfall intensity (I) = 5.193(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.820
Subarea runoff = 0.192(CFS)
Total initial stream area = 0.045(Ac.)

Process from Point/Station 25.000 to Point/Station 26.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.262(CFS)
Depth of flow = 0.160(Ft.), Average velocity = 0.317(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 0.74
 2 12.00 0.50
 3 12.50 0.00
 4 17.50 0.00
 5 18.00 0.50
 Manning's 'N' friction factor = 0.130

 Sub-Channel flow = 0.262(CFS)
 ' ' flow top width = 5.321(Ft.)
 ' ' velocity= 0.317(Ft/s)
 ' ' area = 0.828(Sq.Ft)
 ' ' Froude number = 0.141

Upstream point elevation = 662.300(Ft.)
 Downstream point elevation = 661.400(Ft.)
 Flow length = 95.000(Ft.)
 Travel time = 5.00 min.
 Time of concentration = 8.44 min.
 Depth of flow = 0.160(Ft.)
 Average velocity = 0.317(Ft/s)
 Total irregular channel flow = 0.262(CFS)
 Irregular channel normal depth above invert elev. = 0.160(Ft.)
 Average velocity of channel(s) = 0.317(Ft/s)
 Adding area flow to channel
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [COMMERCIAL area type]
 (General Commercial)
 Impervious value, Ai = 0.850
 Sub-Area C Value = 0.820
 Rainfall intensity = 2.912(In/Hr) for a 2.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.820 CA = 0.094
 Subarea runoff = 0.083(CFS) for 0.070(Ac.)
 Total runoff = 0.275(CFS) Total area = 0.115(Ac.)
 Depth of flow = 0.165(Ft.), Average velocity = 0.322(Ft/s)

 Process from Point/Station 26.000 to Point/Station 27.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

 Upstream point/station elevation = 659.200(Ft.)
 Downstream point/station elevation = 659.000(Ft.)
 Pipe length = 22.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.275(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.275(CFS)
 Normal flow depth in pipe = 3.05(In.)
 Flow top width inside pipe = 6.00(In.)
 Critical Depth = 3.17(In.)
 Pipe flow velocity = 2.74(Ft/s)
 Travel time through pipe = 0.13 min.
 Time of concentration (TC) = 8.58 min.

 Process from Point/Station 27.000 to Point/Station 27.000
 **** SUBAREA FLOW ADDITION ****

 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [COMMERCIAL area type]
 (General Commercial)
 Impervious value, Ai = 0.850

Sub-Area C Value = 0.820
Time of concentration = 8.58 min.
Rainfall intensity = 2.883(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.820 CA = 0.135
Subarea runoff = 0.115(CFS) for 0.050(Ac.)
Total runoff = 0.390(CFS) Total area = 0.165(Ac.)
End of computations, total study area = 0.165 (Ac.)

San Diego County Rational Hydrology Program

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Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 04/02/13

Outfall B
Basin C1
50 Year Rainfall Event

***** Hydrology Study Control Information *****

Program License Serial Number 4012

Rational hydrology study storm event year is 50.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 2.750
24 hour precipitation(inches) = 5.750
P6/P24 = 47.8%
San Diego hydrology manual 'C' values used

Process from Point/Station 24.000 to Point/Station 25.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Initial subarea total flow distance = 75.000(Ft.)
Highest elevation = 663.600(Ft.)
Lowest elevation = 662.300(Ft.)
Elevation difference = 1.300(Ft.) Slope = 1.733 %
Top of Initial Area Slope adjusted by User to 2.034 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 75.00 (Ft)
for the top area slope value of 2.03 %, in a development type of
General Commercial
In Accordance With Figure 3-3
Initial Area Time of Concentration = 3.44 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^{.5}]/(% slope^(1/3))
TC = [1.8*(1.1-0.8200)*(75.000^{.5})/(2.034^(1/3))] = 3.44
Rainfall intensity (I) = 9.214(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.820
Subarea runoff = 0.340(CFS)
Total initial stream area = 0.045(Ac.)

Process from Point/Station 25.000 to Point/Station 26.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.481(CFS)
Depth of flow = 0.231(Ft.), Average velocity = 0.398(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 0.74
 2 12.00 0.50
 3 12.50 0.00
 4 17.50 0.00
 5 18.00 0.50

Manning's 'N' friction factor = 0.130

 Sub-Channel flow = 0.481(CFS)
 ' ' flow top width = 5.462(Ft.)
 ' ' velocity = 0.398(Ft/s)
 ' ' area = 1.208(Sq.Ft)
 ' ' Froude number = 0.149

Upstream point elevation = 662.300(Ft.)
 Downstream point elevation = 661.400(Ft.)
 Flow length = 95.000(Ft.)
 Travel time = 3.98 min.
 Time of concentration = 7.43 min.
 Depth of flow = 0.231(Ft.)
 Average velocity = 0.398(Ft/s)
 Total irregular channel flow = 0.481(CFS)
 Irregular channel normal depth above invert elev. = 0.231(Ft.)
 Average velocity of channel(s) = 0.398(Ft/s)

Adding area flow to channel
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [COMMERCIAL area type]
 (General Commercial)
 Impervious value, Ai = 0.850
 Sub-Area C Value = 0.820
 Rainfall intensity = 5.614(In/Hr) for a 50.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.820 CA = 0.094
 Subarea runoff = 0.189(CFS) for 0.070(Ac.)
 Total runoff = 0.529(CFS) Total area = 0.115(Ac.)
 Depth of flow = 0.245(Ft.), Average velocity = 0.412(Ft/s)

 Process from Point/Station 26.000 to Point/Station 27.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 659.200(Ft.)
 Downstream point/station elevation = 659.000(Ft.)
 Pipe length = 22.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 0.529(CFS)
 Nearest computed pipe diameter = 6.00(In.)
 Calculated individual pipe flow = 0.529(CFS)
 Normal flow depth in pipe = 4.86(In.)
 Flow top width inside pipe = 4.70(In.)
 Critical Depth = 4.45(In.)
 Pipe flow velocity = 3.11(Ft/s)
 Travel time through pipe = 0.12 min.
 Time of concentration (TC) = 7.54 min.

 Process from Point/Station 27.000 to Point/Station 27.000
 **** SUBAREA FLOW ADDITION ****

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [COMMERCIAL area type]
 (General Commercial)
 Impervious value, Ai = 0.850

Sub-Area C Value = 0.820
Time of concentration = 7.54 min.
Rainfall intensity = 5.557(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.820 CA = 0.135
Subarea runoff = 0.222(CFS) for 0.050(Ac.)
Total runoff = 0.752(CFS) Total area = 0.165(Ac.)
End of computations, total study area = 0.165 (Ac.)

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 04/02/13

Outfall C
Basin E
2 Year Rainfall Event

***** Hydrology Study Control Information *****

Program License Serial Number 4012

Rational hydrology study storm event year is 2.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 1.550
24 hour precipitation(inches) = 2.400
P6/P24 = 64.6%
San Diego hydrology manual 'C' values used

Process from Point/Station 28.000 to Point/Station 29.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Initial subarea total flow distance = 75.000(Ft.)
Highest elevation = 661.100(Ft.)
Lowest elevation = 658.800(Ft.)
Elevation difference = 2.300(Ft.) Slope = 3.067 %
Top of Initial Area Slope adjusted by User to 2.154 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 75.00 (Ft)
for the top area slope value of 2.15 %, in a development type of
General Commercial
In Accordance With Figure 3-3
Initial Area Time of Concentration = 3.38 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.8200)*(75.000^0.5)]/(2.154^(1/3))= 3.38
Rainfall intensity (I) = 5.257(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.820
Subarea runoff = 0.319(CFS)
Total initial stream area = 0.074(Ac.)

Process from Point/Station 29.000 to Point/Station 30.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.696(CFS)
Depth of flow = 0.052(Ft.), Average velocity = 1.018(Ft/s)
***** Irregular Channel Data *****

Average velocity of channel(s) = 2.258(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Rainfall intensity = 3.588(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.820 CA = 0.295
Subarea runoff = 0.041(CFS) for 0.032(Ac.)
Total runoff = 1.059(CFS) Total area = 0.360(Ac.)
Depth of flow = 0.077(Ft.), Average velocity = 2.251(Ft/s)
End of computations, total study area = 0.360 (Ac.)

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 04/02/13

Outfall C
Basin E
50 Year Rainfall Event

***** Hydrology Study Control Information *****

Program License Serial Number 4012

Rational hydrology study storm event year is 50.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 2.750
24 hour precipitation(inches) = 5.750
P6/P24 = 47.8%
San Diego hydrology manual 'C' values used

Process from Point/Station 28.000 to Point/Station 29.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Initial subarea total flow distance = 75.000(Ft.)
Highest elevation = 661.100(Ft.)
Lowest elevation = 658.800(Ft.)
Elevation difference = 2.300(Ft.) Slope = 3.067 %
Top of Initial Area Slope adjusted by User to 2.154 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 75.00 (Ft)
for the top area slope value of 2.15 %, in a development type of
General Commercial
In Accordance With Figure 3-3
Initial Area Time of Concentration = 3.38 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^{.5}/(% slope^(1/3))]
TC = [1.8*(1.1-0.8200)*(75.000^{.5})/(2.154^(1/3)]= 3.38
Rainfall intensity (I) = 9.328(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.820
Subarea runoff = 0.566(CFS)
Total initial stream area = 0.074(Ac.)

Process from Point/Station 29.000 to Point/Station 30.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 1.263(CFS)
Depth of flow = 0.065(Ft.), Average velocity = 1.182(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 0.20
 2 50.00 0.00
 3 100.00 0.20

Manning's 'N' friction factor = 0.013

 Sub-Channel flow = 1.263(CFS)
 ' ' flow top width = 32.697(Ft.)
 ' ' velocity= 1.182(Ft/s)
 ' ' area = 1.069(Sq.Ft)
 ' ' Froude number = 1.152

Upstream point elevation = 658.800(Ft.)
 Downstream point elevation = 657.400(Ft.)
 Flow length = 137.000(Ft.)
 Travel time = 1.93 min.
 Time of concentration = 5.31 min.
 Depth of flow = 0.065(Ft.)
 Average velocity = 1.182(Ft/s)
 Total irregular channel flow = 1.263(CFS)
 Irregular channel normal depth above invert elev. = 0.065(Ft.)
 Average velocity of channel(s) = 1.182(Ft/s)
 Adding area flow to channel
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 1.000
 [COMMERCIAL area type]
 (General Commercial)
 Impervious value, Ai = 0.850
 Sub-Area C Value = 0.820
 Rainfall intensity = 6.968(In/Hr) for a 50.0 year storm
 Effective runoff coefficient used for total area
 (Q=KCIA) is C = 0.820 CA = 0.269
 Subarea runoff = 1.308(CFS) for 0.254(Ac.)
 Total runoff = 1.874(CFS) Total area = 0.328(Ac.)
 Depth of flow = 0.076(Ft.), Average velocity = 1.304(Ft/s)

 Process from Point/Station 30.000 to Point/Station 31.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

 Estimated mean flow rate at midpoint of channel = 1.966(CFS)
 Depth of flow = 0.112(Ft.), Average velocity = 2.865(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 0.50
 2 0.50 0.00
 3 6.50 0.00
 4 7.00 0.50

Manning's 'N' friction factor = 0.013

 Sub-Channel flow = 1.966(CFS)
 ' ' flow top width = 6.225(Ft.)
 ' ' velocity= 2.865(Ft/s)
 ' ' area = 0.686(Sq.Ft)
 ' ' Froude number = 1.521

Upstream point elevation = 657.400(Ft.)
 Downstream point elevation = 656.600(Ft.)
 Flow length = 66.000(Ft.)
 Travel time = 0.38 min.
 Time of concentration = 5.70 min.
 Depth of flow = 0.112(Ft.)
 Average velocity = 2.865(Ft/s)
 Total irregular channel flow = 1.966(CFS)
 Irregular channel normal depth above invert elev. = 0.112(Ft.)

Average velocity of channel(s) = 2.865(Ft/s)
Adding area flow to channel
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Rainfall intensity = 6.661(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for total area
(Q=KCIA) is C = 0.820 CA = 0.295
Subarea runoff = 0.092(CFS) for 0.032(Ac.)
Total runoff = 1.966(CFS) Total area = 0.360(Ac.)
Depth of flow = 0.112(Ft.), Average velocity = 2.865(Ft/s)
End of computations, total study area = 0.360 (Ac.)

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 04/02/13

Outfall D
Basin E1
2 Year Rainfall Event

***** Hydrology Study Control Information *****

Program License Serial Number 4012

Rational hydrology study storm event year is 2.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 1.550
24 hour precipitation(inches) = 2.400
P6/P24 = 64.6%
San Diego hydrology manual 'C' values used

Process from Point/Station 28.000 to Point/Station 32.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Initial subarea total flow distance = 83.000(Ft.)
Highest elevation = 661.100(Ft.)
Lowest elevation = 658.300(Ft.)
Elevation difference = 2.800(Ft.) Slope = 3.373 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 85.00 (Ft)
for the top area slope value of 3.37 %, in a development type of
General Commercial
In Accordance With Figure 3-3
Initial Area Time of Concentration = 3.10 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^{.5}/(% slope^(1/3))]
TC = [1.8*(1.1-0.8200)*(85.000^{.5})/(3.373^(1/3))] = 3.10
Rainfall intensity (I) = 5.561(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.820
Subarea runoff = 0.360(CFS)
Total initial stream area = 0.079(Ac.)
End of computations, total study area = 0.079 (Ac.)

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 04/02/13

Outfall D
Basin E1
50 Year Rainfall Event

***** Hydrology Study Control Information *****

Program License Serial Number 4012

Rational hydrology study storm event year is 50.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 2.750
24 hour precipitation(inches) = 5.750
P6/P24 = 47.8%
San Diego hydrology manual 'C' values used

Process from Point/Station 28.000 to Point/Station 32.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Initial subarea total flow distance = 83.000(Ft.)
Highest elevation = 661.100(Ft.)
Lowest elevation = 658.300(Ft.)
Elevation difference = 2.800(Ft.) Slope = 3.373 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 85.00 (Ft)
for the top area slope value of 3.37 %, in a development type of
General Commercial
In Accordance With Figure 3-3
Initial Area Time of Concentration = 3.10 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^{0.5}]/(% slope^{1/3})
TC = [1.8*(1.1-0.8200)*(85.000^{0.5})/(3.373^{1/3})] = 3.10
Rainfall intensity (I) = 9.866(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.820
Subarea runoff = 0.639(CFS)
Total initial stream area = 0.079(Ac.)
End of computations, total study area = 0.079 (Ac.)

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 04/02/13

Outfall E
Basin B1
2 Year Rainfall Event

***** Hydrology Study Control Information *****

Program License Serial Number 4012

Rational hydrology study storm event year is 2.0
English (in-lb) input data Units used

Map data precipitation entered:
6 hour, precipitation(inches) = 1.550
24 hour precipitation(inches) = 2.400
P6/P24 = 64.6%
San Diego hydrology manual 'C' values used

Process from Point/Station 33.000 to Point/Station 34.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Initial subarea total flow distance = 67.000(Ft.)
Highest elevation = 661.700(Ft.)
Lowest elevation = 660.200(Ft.)
Elevation difference = 1.500(Ft.) Slope = 2.239 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 75.00 (Ft)
for the top area slope value of 2.24 %, in a development type of
General Commercial
In Accordance With Figure 3-3
Initial Area Time of Concentration = 3.34 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^{.5}]/(% slope^(1/3))
TC = [1.8*(1.1-0.8200)*(75.000^{.5})/(2.239^(1/3))] = 3.34
Rainfall intensity (I) = 5.301(In/Hr) for a 2.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.820
Subarea runoff = 0.204(CFS)
Total initial stream area = 0.047(Ac.)
End of computations, total study area = 0.047 (Ac.)

San Diego County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c)1991-2004 Version 7.4

Rational method hydrology program based on
San Diego County Flood Control Division 2003 hydrology manual
Rational Hydrology Study Date: 04/02/13

Outfall E
Basin Bl
50 Year Rainfall Event

***** Hydrology Study Control Information *****

Program License Serial Number 4012

Rational hydrology study storm event year is 50.0
English (in-lb) input data Units used

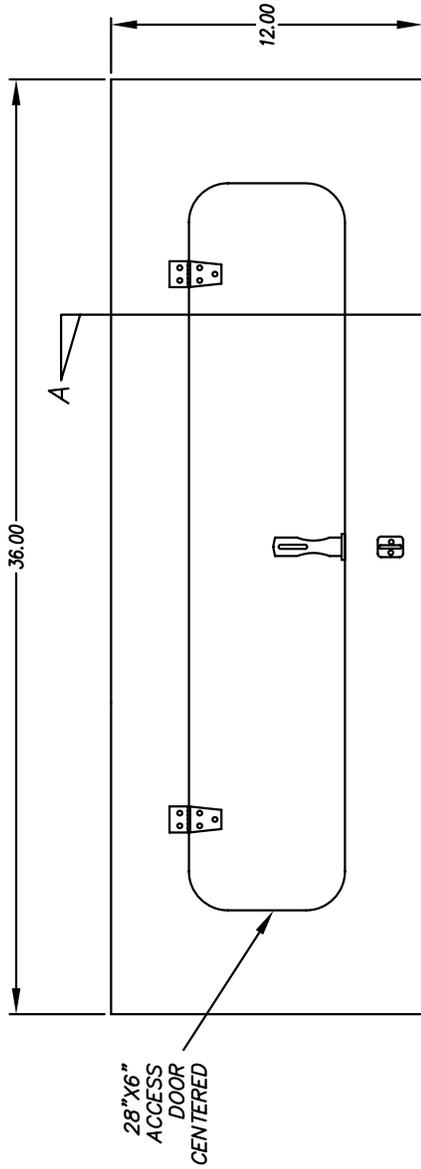
Map data precipitation entered:
6 hour, precipitation(inches) = 2.750
24 hour precipitation(inches) = 5.750
P6/P24 = 47.8%
San Diego hydrology manual 'C' values used

Process from Point/Station 33.000 to Point/Station 34.000
**** INITIAL AREA EVALUATION ****

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
[COMMERCIAL area type]
(General Commercial)
Impervious value, Ai = 0.850
Sub-Area C Value = 0.820
Initial subarea total flow distance = 67.000(Ft.)
Highest elevation = 661.700(Ft.)
Lowest elevation = 660.200(Ft.)
Elevation difference = 1.500(Ft.) Slope = 2.239 %
INITIAL AREA TIME OF CONCENTRATION CALCULATIONS:
The maximum overland flow distance is 75.00 (Ft)
for the top area slope value of 2.24 %, in a development type of
General Commercial
In Accordance With Figure 3-3
Initial Area Time of Concentration = 3.34 minutes
TC = [1.8*(1.1-C)*distance(Ft.)^0.5]/(% slope^(1/3))
TC = [1.8*(1.1-0.8200)*(75.000^0.5)]/(2.239^(1/3))= 3.34
Rainfall intensity (I) = 9.406(In/Hr) for a 50.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.820
Subarea runoff = 0.362(CFS)
Total initial stream area = 0.047(Ac.)
End of computations, total study area = 0.047 (Ac.)

ATTACHMENT F
BIO CLEAN FLUME FILTER

BIO CLEAN FLUME FILTER – 36 INCH – MEDIA TYPE

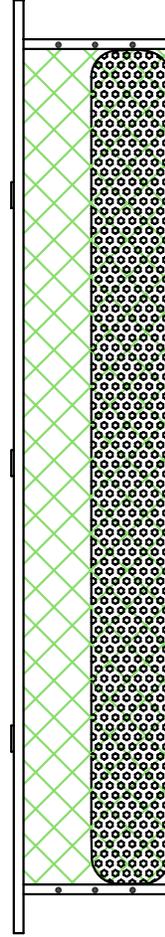
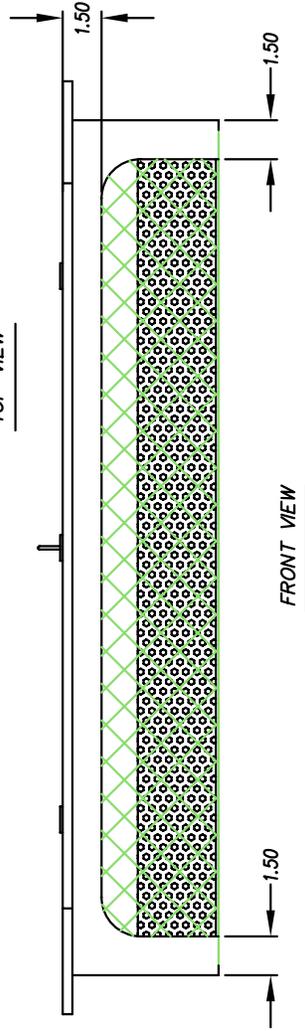
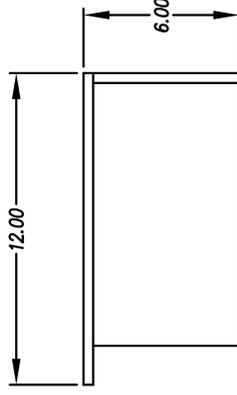


3/4" STARBOARD

3" DIA. BIOSORB HYDROCARBON BOOMS MADE OF 100% POLYESTER NETTED FABRIC CONTAINING BIOSORB HYDROCARBON ABSORBING MEDIA.

STAINLESS STEEL EXPANDED METAL

SECTION A-A



5 YEAR MANUFACTURERS WARRANTY

PATENTED

ALL FILTER SCREENS ARE STAINLESS STEEL

P 760-433-7640 F 760-433-3176

EMAIL: info@biocleanenvironmental.net

TREATMENT FLOW RATE = .26 CFS PER LINEAR FOOT FLOW RATE ASSUMES 50% BLOCKAGE

TREATMENT FLOW RATE = .78 CFS

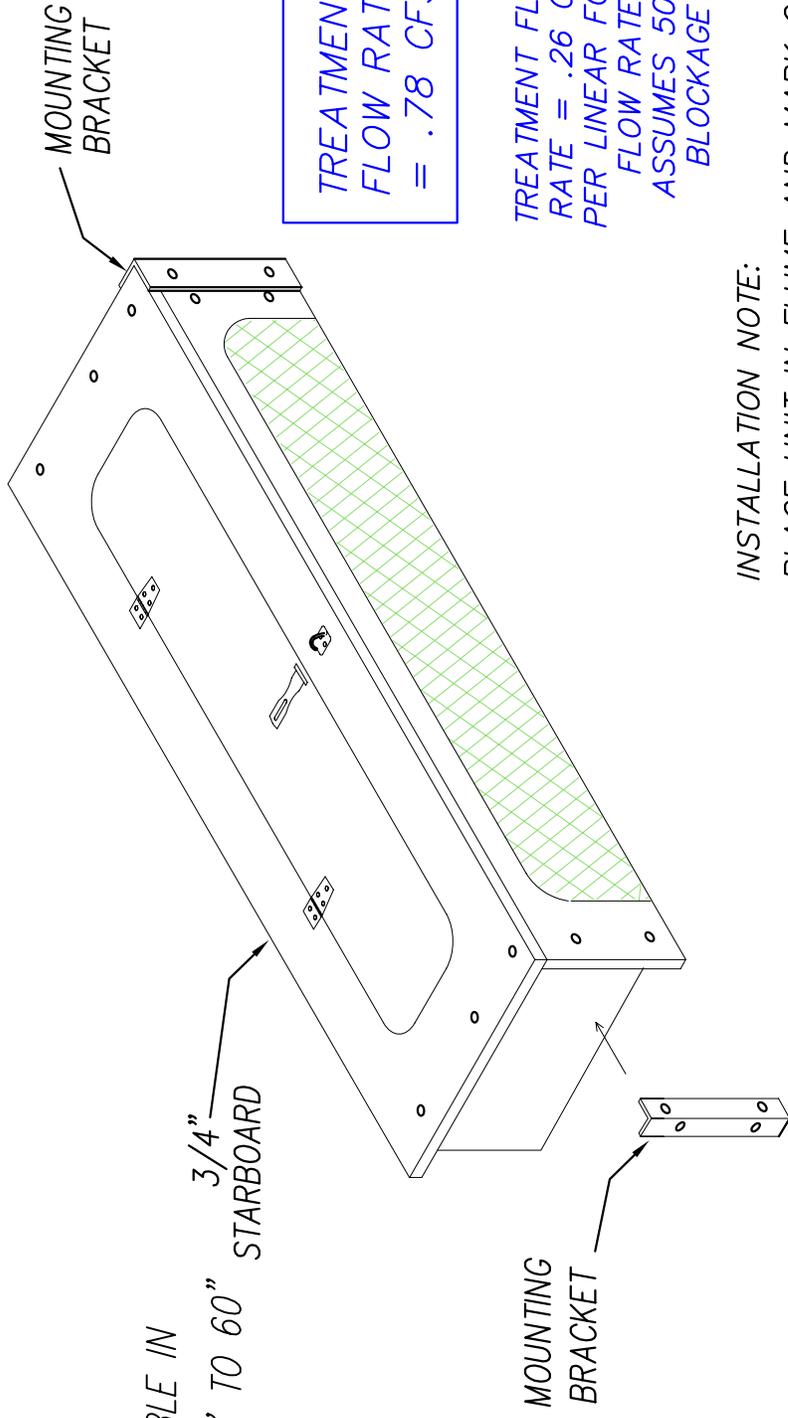


BIO CLEAN
ENVIRONMENTAL SERVICES, INC.

| | | | |
|-------|----------|---|--------|
| SIZE | FSCM NO. | DWG NO. | REV |
| | | BIO CLEAN FLUME FILTER 36" – MEDIA TYPE | |
| SCALE | N. T. S. | SHEET | 1 OF 2 |

BIO CLEAN FLUME FILTER – 36 INCH – MEDIA TYPE

THIS FILTER IS AVAILABLE IN SIZES RANGING FROM 12" TO 60"



TREATMENT FLOW RATE = .78 CFS

TREATMENT FLOW RATE = .26 CFS PER LINEAR FOOT FLOW RATE ASSUMES 50% BLOCKAGE

INSTALLATION NOTE:

PLACE UNIT IN FLUME AND MARK CONCRETE FOR MOUNTING ANGLES. INSTALL ANGLES, THEN PLACE UNIT ON MOUNTING ANGLES AND INSTALL WITH 2" X #8 SCREWS.

THE BIOSORB MATERIAL IS MADE OF A PROPRIETARY POLYMER BASED BEADS. THE MATERIAL IS USUALLY CONTAINED WITHIN BOOMS OR POUCHES. THE BOOMS AND POUCHES ARE MADE OF 100% POLYESTER NETTED FABRIC WITH SIEVE OPENINGS 1mm, OPEN AREA RATIO IS APPROXIMATELY 67%. THE BIOSORB AND NETTING ARE OF SUFFICIENT STRENGTH TO SUPPORT WATER, SEDIMENT, AND DEBRIS LOADS WHEN THE MEDIA IS AT MAXIMUM ABSORPTION CAPACITY, WITH NO SLIPPAGE, BREAKING, OR TEARING. THE BIOSORB HAS BEEN TESTED THROUGH RIGOROUS FLOW AND LOADING CONDITIONS. THE BIOSORB IS DESIGNED TO CAPTURE HIGH LEVELS OF HYDROCARBONS INCLUDING BUT NOT LIMITED TO OILS AND GREASE, GASOLINE, DIESEL, AND PAHS. THE GRANULE NATURE OF THE MATERIAL, WITH APPROXIMATELY 2000MM SIZED GRANULES ALSO HAS THE PHYSICAL ABILITY TO BLOCK AND FILTER TRASH AND LITTER, GRASS AND FOLIAGE, AND SEDIMENTS.

P 760-433-7640 F 760-433-3176
EMAIL: info@biocleanenvironmental.net



| | | | |
|-------|----------|---|--------|
| SIZE | FSCM NO. | DWG NO. | REV |
| | | BIO CLEAN FLUME FILTER 36" – MEDIA TYPE | |
| SCALE | N. T. S. | SHEET | 2 OF 2 |